



**Audio Engineering Society**

**PNW Section 24 May 2005**

# Real-World Balanced Interfaces and Other-World Myths

Presented by  
**Bill Whitlock**

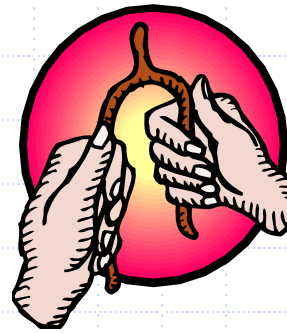
President, Jensen Transformers, Inc.

Member, Audio Engineering Society  
Senior Member, Institute of Electrical and Electronic Engineers

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# So Many Myths

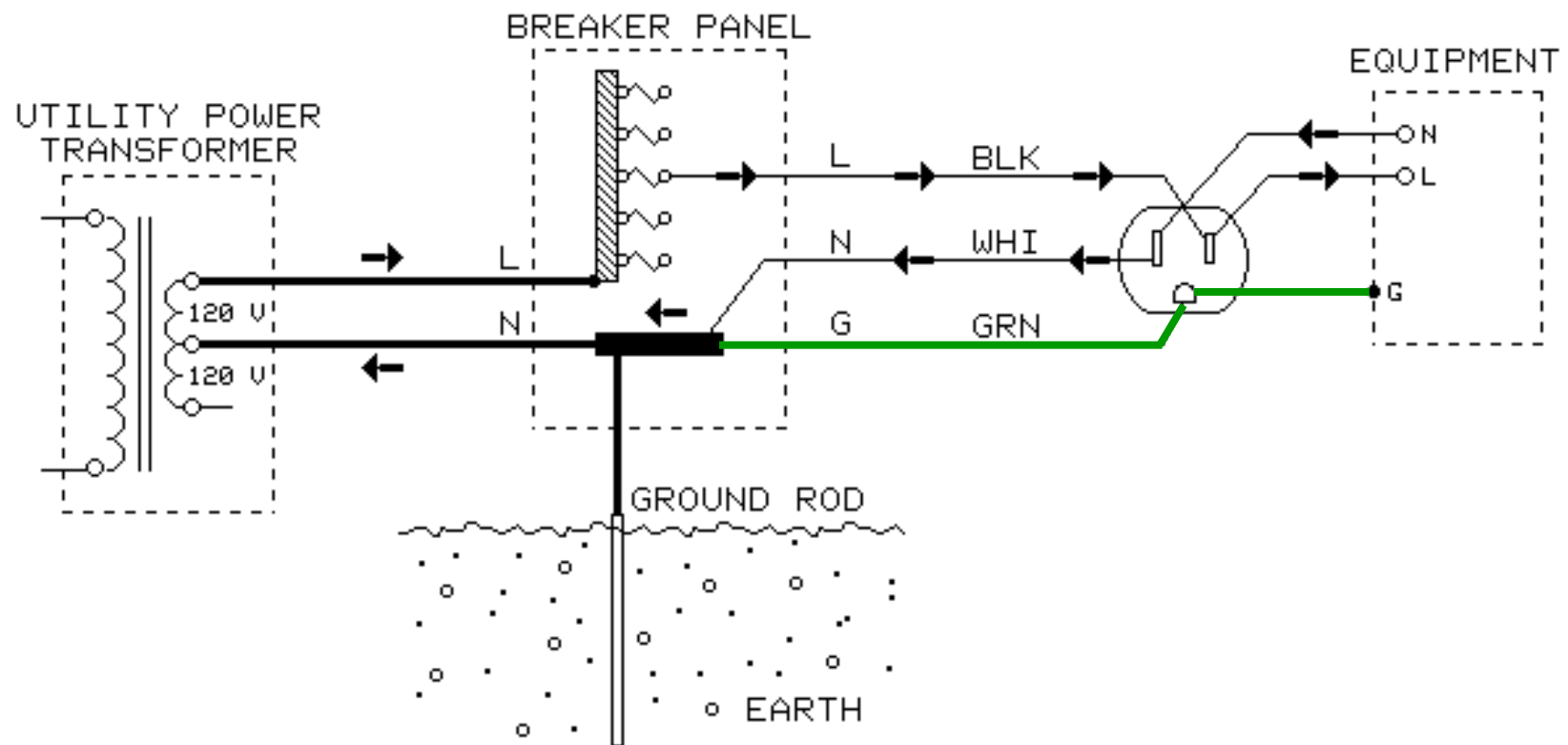
- Look for **MYTH** alerts ...
- Topic has "BLACK ART" reputation
- Basic rules of physics are routinely overlooked, ignored, or forgotten
- Manufacturers often clueless – don't know ground loops from



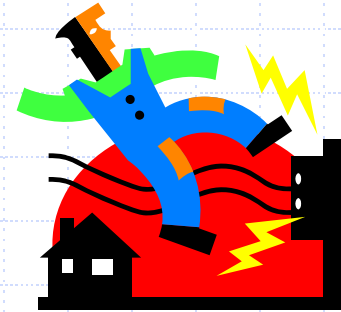
# The Electrical Environment

- Regulations protecting us from electrocution and fire also play a big role in noise problems
- NEC or “Code” requires 120-volt ac power distribution via a 3-wire system
- **Safety Grounding** electrically interconnects conductive objects to keep voltages between them safe, *even if equipment fails ...*
- Neutral (white) and safety ground (green) are bonded together at service entrance only

# Normal Load Current in Branch Circuit



# Deadly Equipment

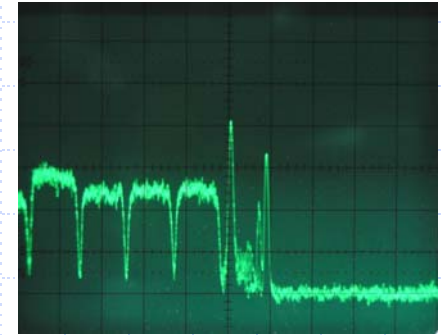


- Equipment can become a shock/electrocution hazard if its internal insulation fails
- Such a defect can make the entire device “live” at 120 volts and is called a **FAULT**
- Without a safety ground, these failures can shock or electrocute people or start fires!
- Signal cables conduct 120 volts – **one FAULT can turn an entire system into a shock hazard**

# Don't Electrocute System Users!!



# Shock and Electrocution

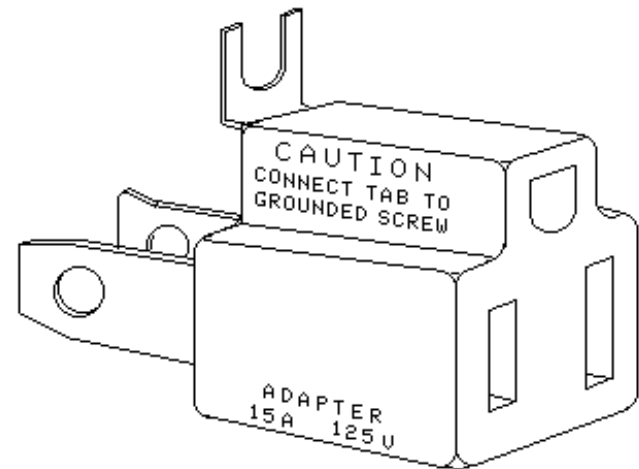


- **CURRENT** determines severity
  - Under 1 mA causes just an unpleasant “tingling”
  - About 10 mA causes involuntary muscle contraction and “death grip” or suffocation if through chest
  - Over 50 mA through chest can induce ventricular fibrillation – causing brain death minutes later
- Dry skin has high resistance – keeping current low when lightly touching a 120-volt wire
- Skin moisture, larger contact area, or increased pressure will substantially increase current
- **Always respect the dangers of electricity!**

# DON'T BET YOUR LIFE!

*NEVER, EVER defeat safety grounding to solve a noise problem!*

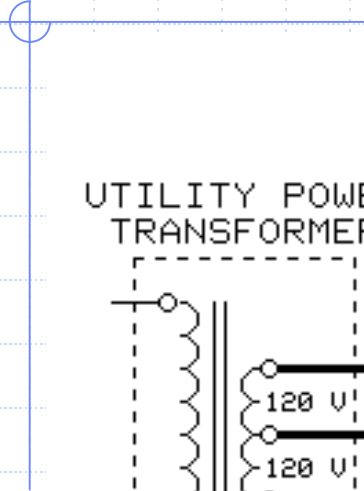
This adapter is intended to **PROVIDE** safety grounding for a 2-prong receptacle (via its cover mounting screw, metallic saddle, J-box, and conduit back to breaker box)





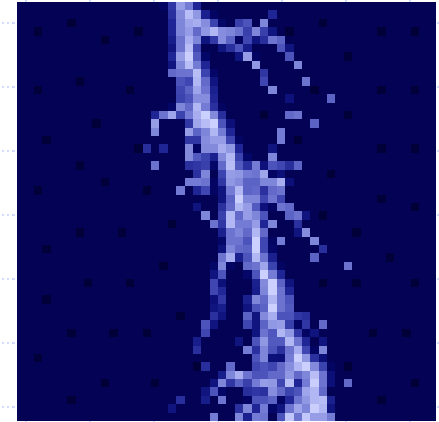
# MYTH: Safety Grounds Work Because of Earth Grounding

- Safety ground is bonded to **NEUTRAL** at main entry panel
- This low-impedance circuit allows high fault current, tripping breaker quickly
- Earth ground does **NOT** play a role!



# Earth Ground is for LIGHTNING

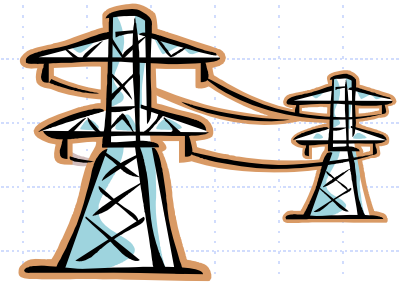
- Power lines become targets of ...
- Before Code, power lines literally guided lightning into buildings!
- Outdoor power lines grounded at intervals
- Impedance of ground rod at service entrance is  $<25\ \Omega$ , sufficient to limit lightning damage
- Protection of phone and CATV lines, where they enter building, is also required by Code



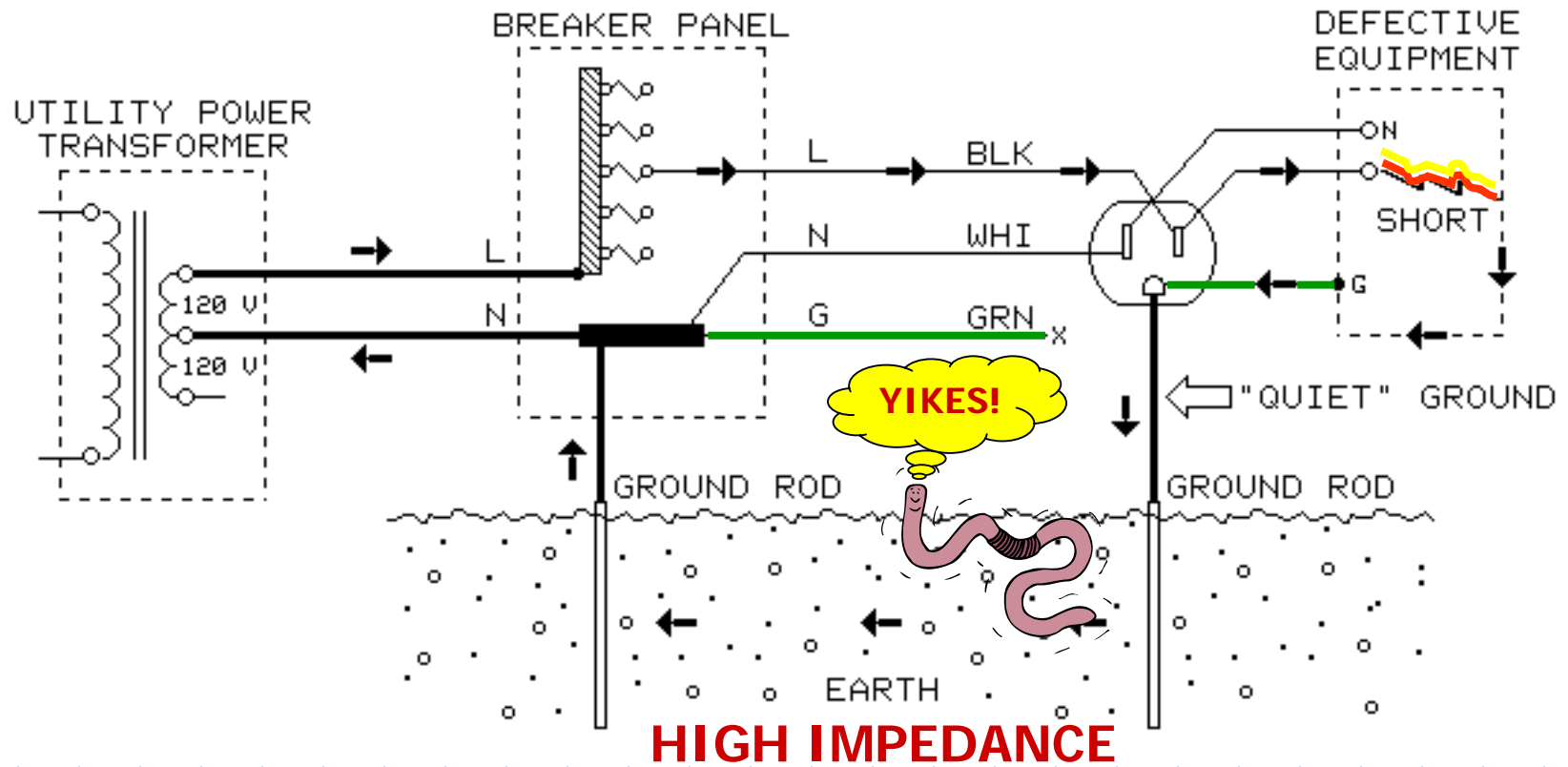
# MYTH: Earth Ground = Zero Volts

- NOT with respect to each other or some mystical "absolute" reference point
- Other nearby ground connections create soil voltage gradients
- "Those looking for a better earth or better ground to solve a noise problem are looking for pie in the sky."

Ralph Morrison



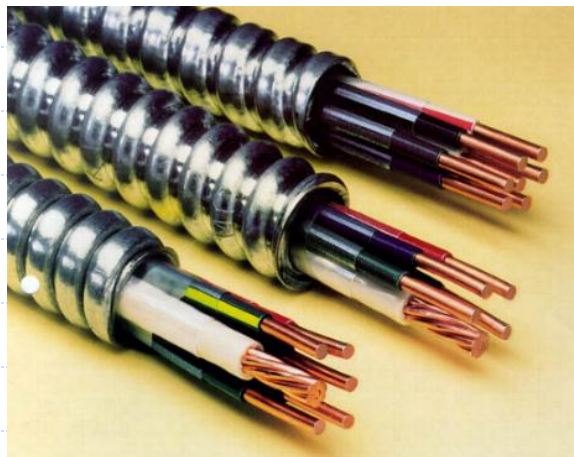
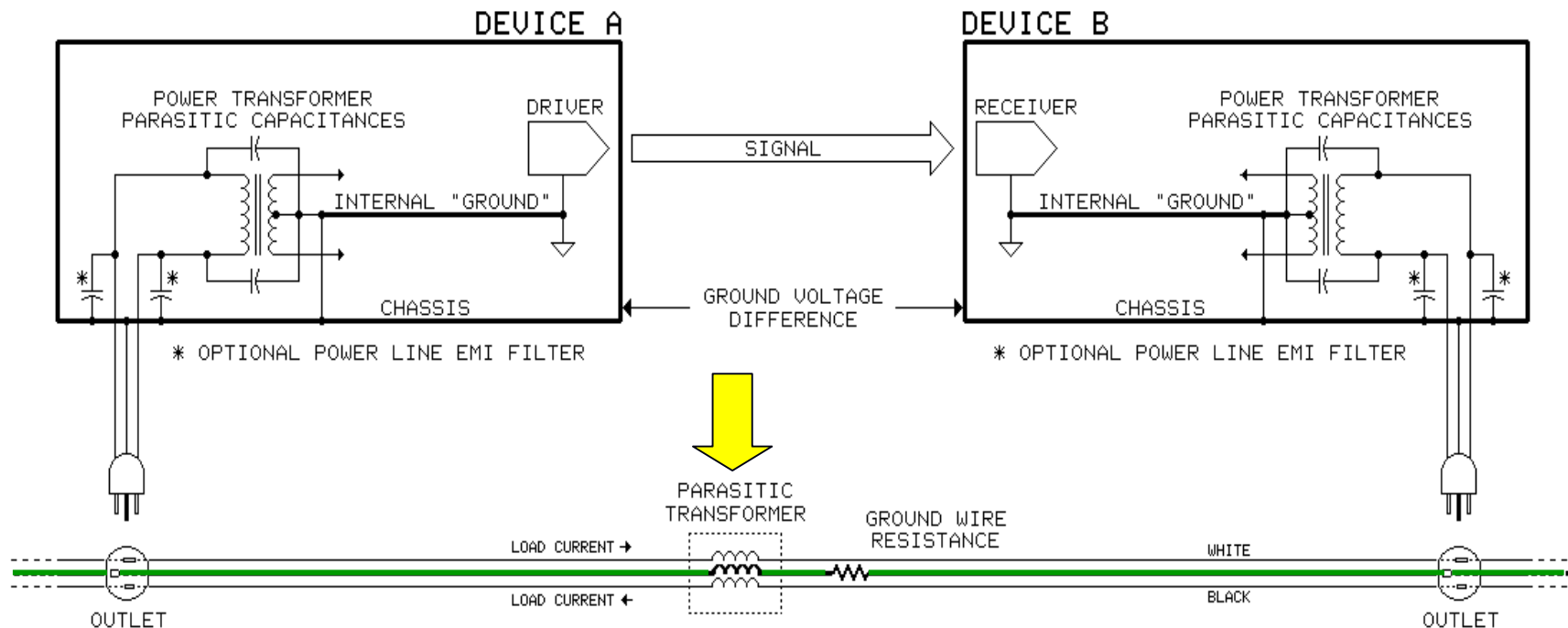
# Ground Rod is **Useless** for Fault Currents



# MYTH: Most Noise is Caused by “Improper” AC Power Wiring

- Small voltages between outlet safety grounds is **NORMAL** in proper wiring
  - Parasitic transformer effects in wiring
  - Lowest between nearby outlets on the same branch circuit
  - Highest (up to a few volts) between distant outlets on different branch circuits
- **INTERFACE problems cause the NOISE!**

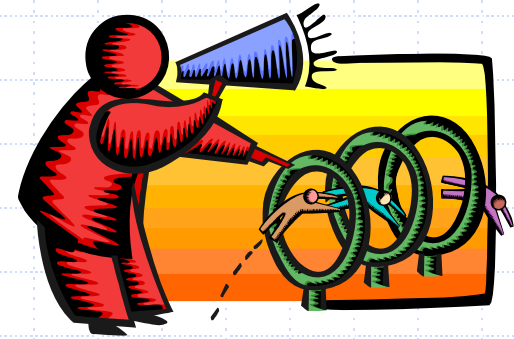
# The Parasitic Transformer



Load current magnetically induces voltage in ground wiring between outlets

*Copper Institute*

# About 2-prong Plugs

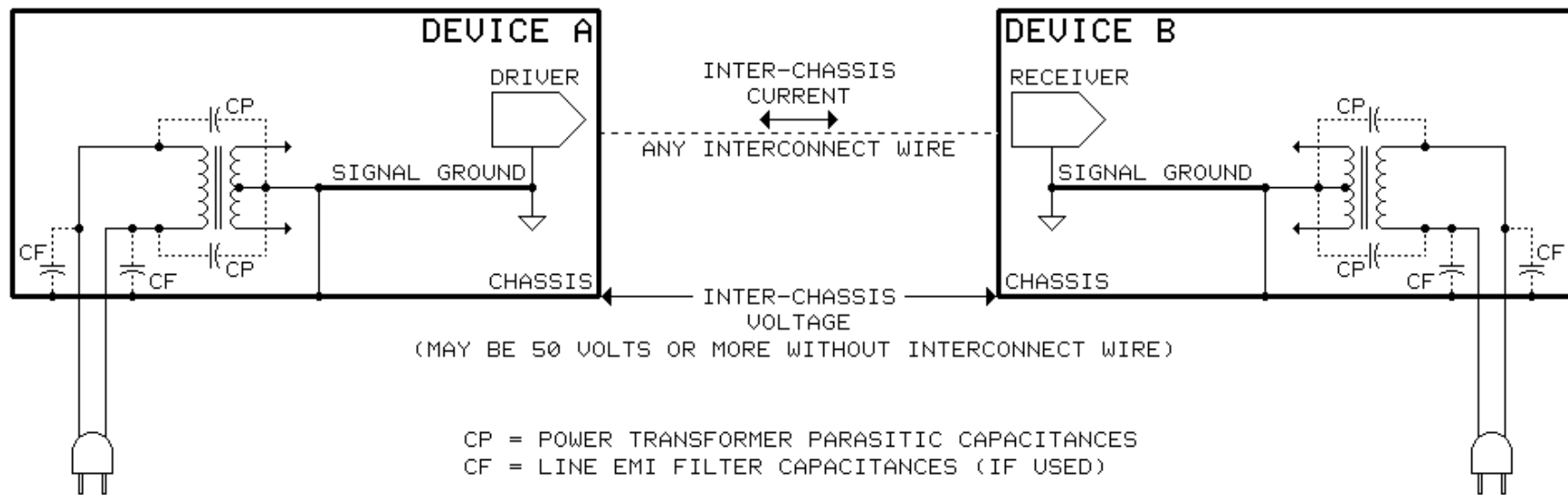


- UL approval requires extraordinary protection
  - Must remain safe in spite of component failure, overload, and rough handling
- Chassis voltage can approach 120 volts but current is limited by parasitic capacitances
  - 0.75 mA maximum for consumer electronics
- This "**LEAKAGE**" current will flow in signal cables connected to other equipment





# Equipment with 2-prong Plugs



**LEAKAGE** current flows in signal cables between devices with 2-prong ac plugs

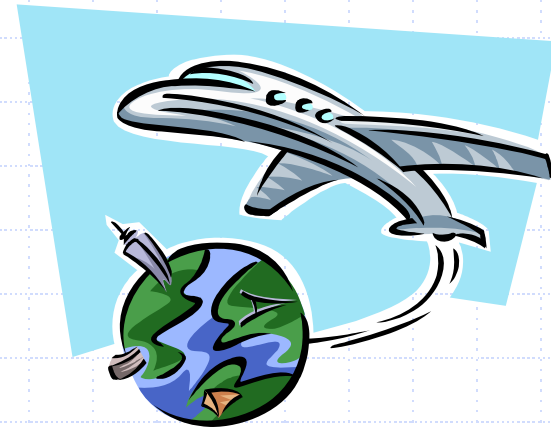
# The Facts Of Life



- Ground voltage differences will **ALWAYS** exist between outlets
- Leakage currents will **ALWAYS** flow in signal cables
- **COUPLING** allows them to enter the signal path and is the REAL problem!

# MYTH: These Voltages and Currents can be Eliminated

- “SHORT ‘EM OUT” with massive copper bus bars
- Experiment to find a “better” or “quieter” ground
- Route noise to an **earth** ground where it disappears
- Make the electrician fix “his” problem
- Install equipment to “purify” the “dirty” ac power
- Does an earth ground really stop noise? Think about all the electronics in a 747 ...



# Think “Outside the Box”

- **SIGNALS** accumulate **NOISE** as they flow through a system
- Removing noise without altering/degrading the signal is essentially impossible
- Entire signal path must prevent noise coupling
- Signal **INTERFACES** are the danger zone, rather than the equipment itself
- *"A cable is a source of potential trouble connecting two other sources of potential trouble."*

# What's an Interface?

- Signal transport sub-system consisting of a line **DRIVER** (output), the **LINE** or cable, and a line **RECEIVER** (input)
- **TWO** conductors are always required to complete a signal (or any) current path

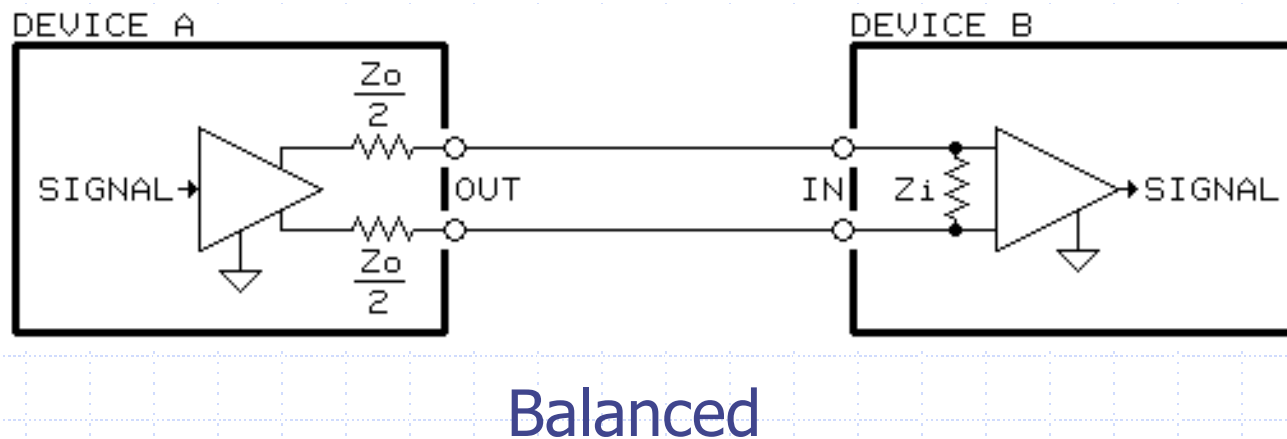
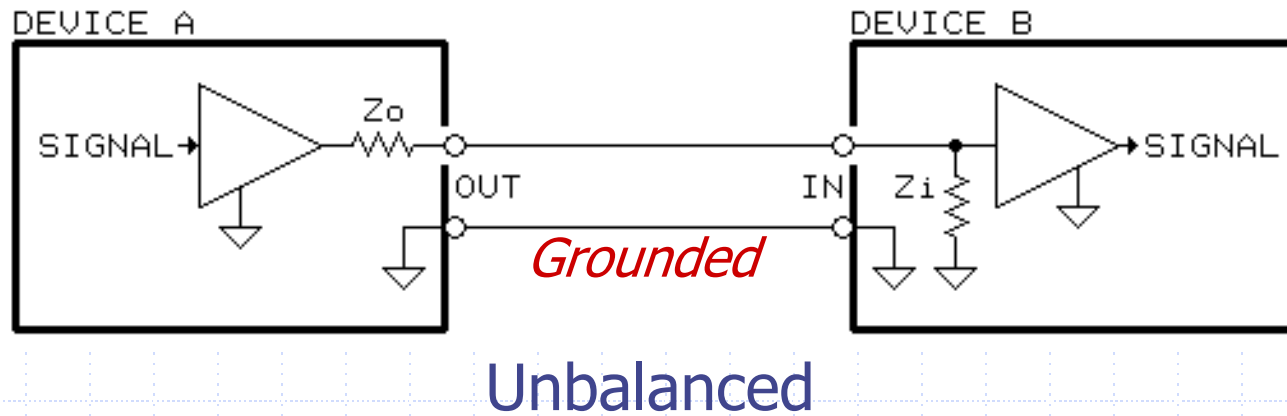
# What's Impedance?

- The apparent resistance to current flow in an AC circuit – *the functional equivalent of resistance in a DC circuit*
- Symbolized **Z** and measured in ohms

# Balanced and Unbalanced

- Status depends **ONLY** on the **IMPEDANCES** (to ground) of the two signal conductors
- In **UN**balanced interface, one has zero impedance (grounded) and other has some higher impedance
- In balanced interface, both have nominally **equal** impedances
  - Requires that driver, line, and receiver each maintain equal impedances

# Unbalanced vs Balanced Interfaces





# Driver & Receiver Impedances

- Every **driver** has an internal impedance called **output impedance**, shown as  $Z_o$ 
  - Real outputs can't have zero output impedance, but lower is better
  - Often confused with **load** impedance
- Every **receiver** has an internal impedance called **input impedance**, shown as  $Z_i$ 
  - Real inputs can't have infinite input impedance, but higher is better

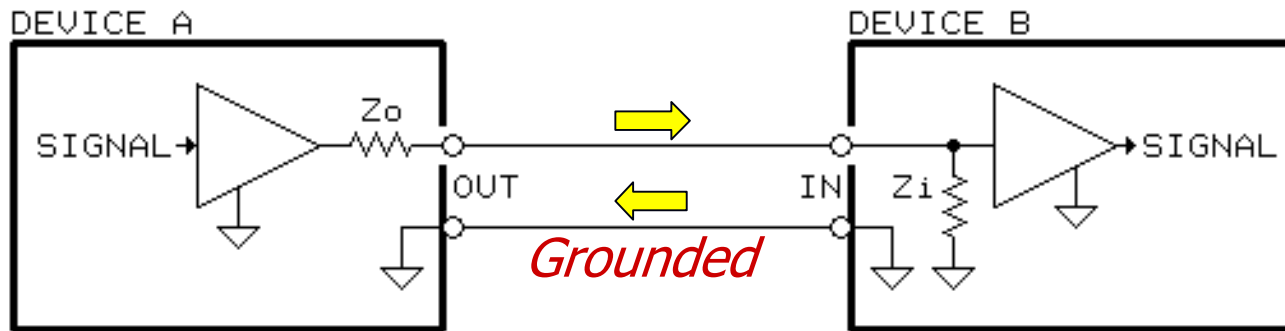
# MYTH: Impedance Implies Level

- Signal level, impedance, and balance are completely independent of each other:
  - Pro Mic out = lo-Z, lo-level, balanced
  - Pro Line out = lo-Z, hi-level, balanced
  - Consumer/MI Line out = lo-Z, hi-level, unbalanced
  - Consumer Mic out = lo-Z, lo-level, unbalanced
  - Phono out = hi-Z, lo-level, unbalanced
  - Guitar out = hi-Z, hi-level, unbalanced

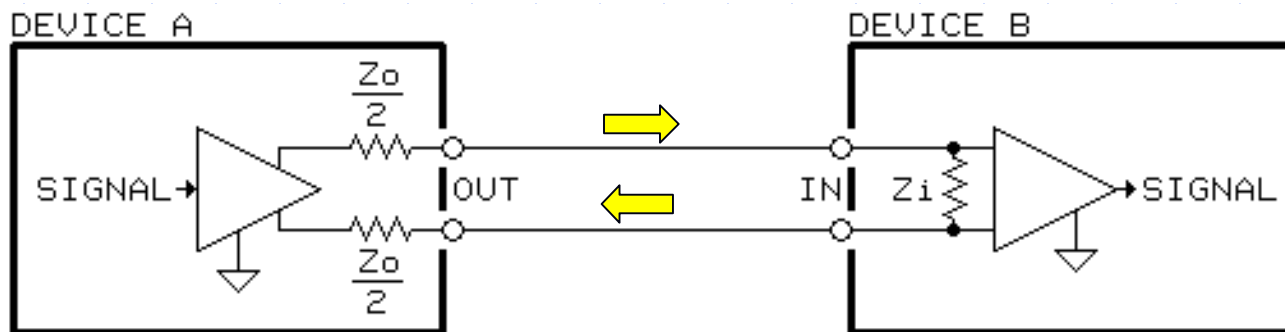
# A Signal Voltage Divider

- Driver and receiver impedances  $Z_o$  and  $Z_i$  form **series circuit** called a voltage divider
- Voltage drops are proportional to impedance
- For maximum signal **voltage** at receiver,  $Z_i$  must be much greater than  $Z_o$
- Typical audio interfaces transfer 90% to 99.9% of the available signal voltage

# The Signal Voltage Divider



Unbalanced



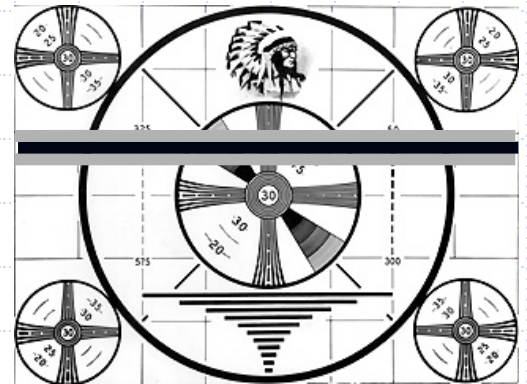
Balanced

# MYTH: Audio Inputs and Outputs Should Be "Impedance Matched"

- Wastes half the signal voltage and places an unnecessarily heavy load on the driver!
- Transfers maximum **power** (vintage passive systems) but not applicable to modern audio systems driven by signal **voltage**
  - Video and higher frequency cables are impedance matched to avoid "transmission line" effects
  - **AUDIO** cables about 4,000 feet long only begin to exhibit very slight transmission line effects!

# UNBALANCED Interfaces

- **EXTREMELY** susceptible to noise coupling!
- Ironical that, after 50 years, they remain the norm in consumer and audiophile audio, even as dynamic range requirements have steadily increased
- **Video** interfaces (analog)
  - Coupling causes visible "hum bars"
- **RS-232** interfaces
  - Coupling causes "mysterious" problems

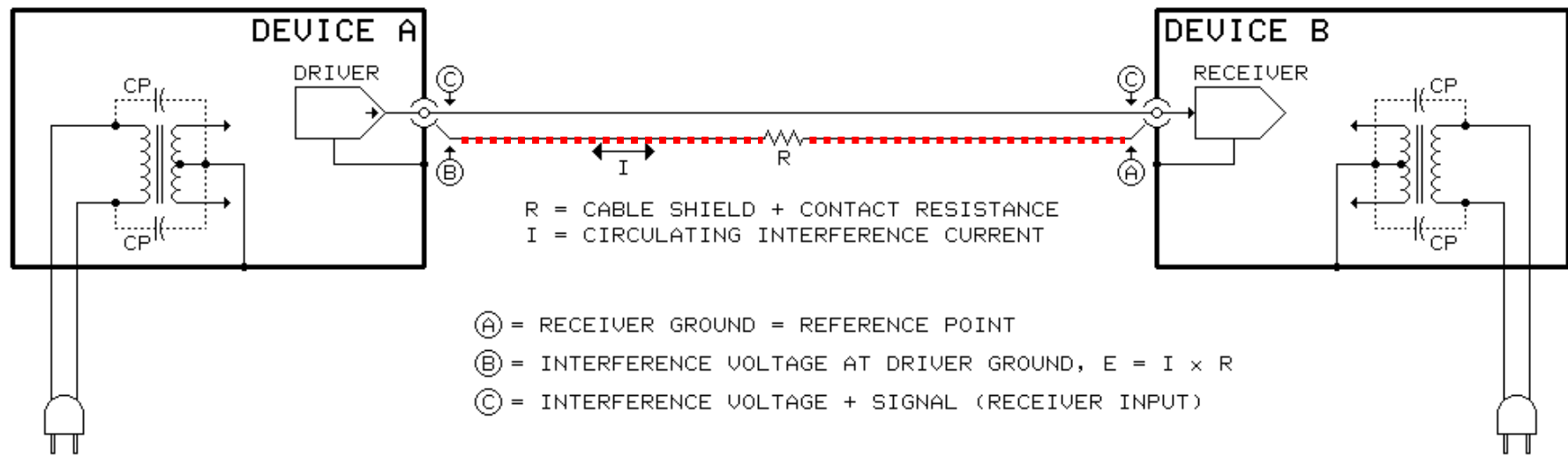


# The Big Problem

- Leakage currents flow in signal cables
  - Virtually all in grounded conductor, typically the “shield,” whose impedance is not zero
- Noise voltage generated over its length due to its resistance – Ohm’s Law
- Noise **directly adds to signal** seen at receiver (voltages add in series circuit)

# Common-Impedance Coupling

It's **NOT** about SHIELDING!





# MYTH: Poor Shielding Causes Noise

- Common-impedance coupling causes 99% of noise problems in unbalanced interfaces
- Trivial noise contributor in modern systems
- Audiophile cables from famous maker, costing \$80 to \$500 per 1-meter pair, have no shield at all — wires are simply woven together!
- Shielding can be issue with old vacuum-tube equipment because of high  $Z_o$  in drivers

# A Real-World Example

- Assume 25-foot, foil-shield cable with #26 AWG drain wire,  $R = 1\ \Omega$
- Assume leakage current between 2-prong (ungrounded) devices is  $316\ \mu\text{A}$
- Noise voltage =  $316\ \mu\text{V}$
- Consumer reference =  $316\ \text{mV}$
- S/N ratio =  $316\ \text{mV}/316\ \mu\text{V} = \text{only } 60\ \text{dB}$
- Belden #8241F cable, shield  $R = 0.065\ \Omega$ , would improve S/N by some 24 dB!

# From Bad to Worse ...

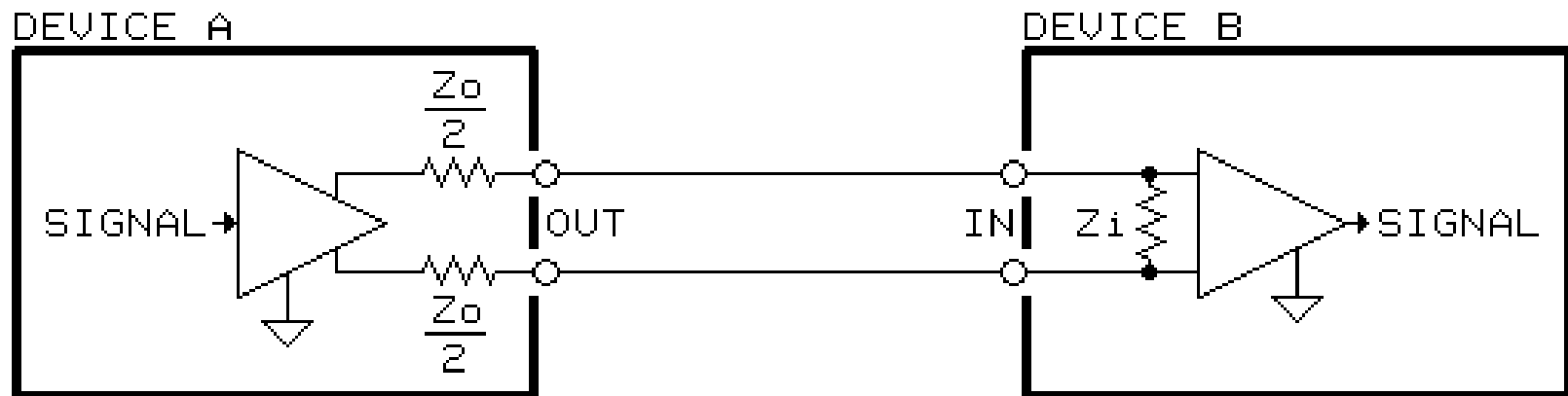
- When devices are grounded, often via other system cables, noise can become **EXTREME!**
  - When ground voltage difference of only 30 mV between outlets is impressed across length of cable, resulting S/N becomes only **20 dB**
  - **Huge problem in home theater systems having multiple ground connections** – sub-woofers and projectors with 3-prong plugs, CATV, and satellite TV connections

# MYTH: Expensive Cables Stop Noise

Exotic cables, even if double or triple shielded, made of 100% pure unobtainium, and hand woven by a team of virgins will have no significant effect on hum and buzz!

Only shield resistance makes a difference!

# BALANCED Interfaces



- **THE ULTIMATE** in noise prevention!
- The only technique used in telephone systems

# MYTH: Balance = Signal Symmetry

Example from "white paper" at well-known manufacturer's website:

"Each conductor is always equal in voltage but opposite in polarity to the other. The circuit that receives this signal in the mixer is called a differential amplifier and this opposing polarity of the conductors is essential for its operation."

Not only **WRONG** but it misses the truly essential feature of a balanced interface

# The Real Definition

"A balanced circuit is a **two-conductor** circuit in which both conductors and all circuits connected to them have the **same impedance with respect to ground** and to all other conductors. The purpose of balancing is to make the noise pickup equal in both conductors, in which case it will be a common-mode signal which can be made to cancel out in the load."

- Henry Ott

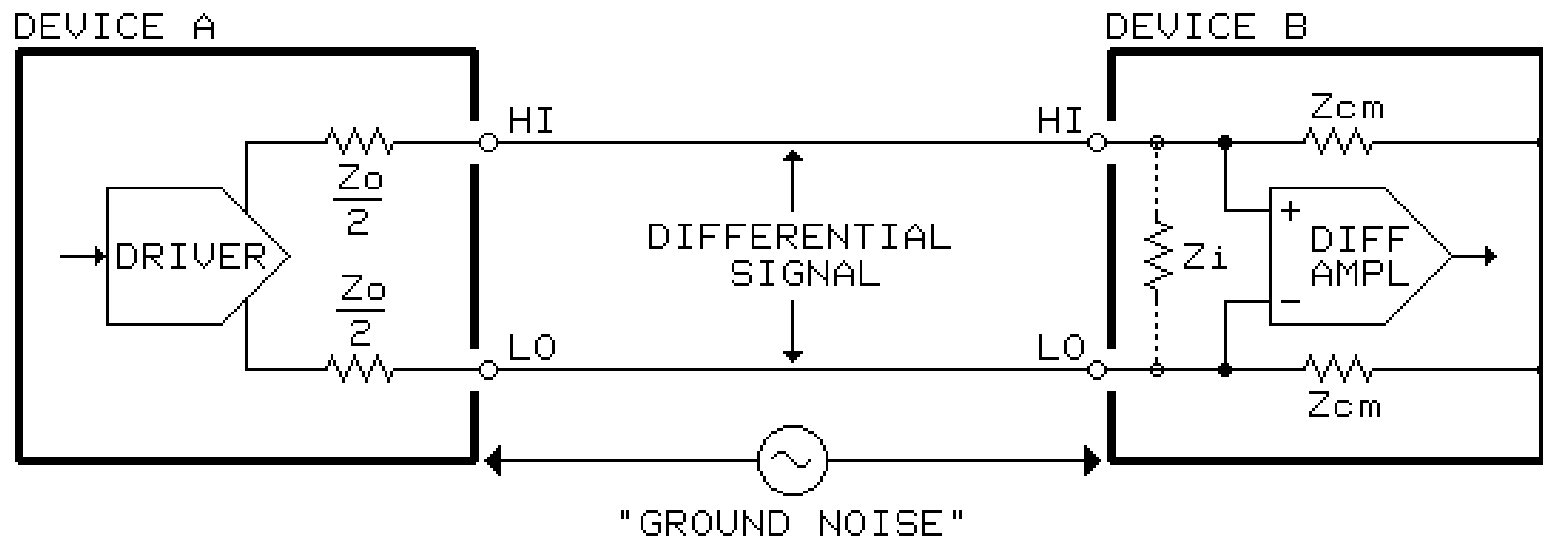
# Furthermore ...

“Only the common-mode impedance balance of the driver, line, and receiver play a role in noise or interference rejection. This noise or interference rejection property is independent of the presence of a desired differential signal. Therefore, **it can make no difference whether the desired signal exists entirely on one line, as a greater voltage on one line than the other, or as equal voltages on both of them.** Symmetry of the desired signal has advantages, but they concern headroom and crosstalk, not noise or interference rejection.”

*from "Informative Annex" of IEC Standard 60268-3*



# The Basic Concept



Any interference that creates identical voltages at the receiver inputs is rejected

# The History of Balanced Lines

- Bell Telephone pioneered use
- Early systems passive – no amplifiers
- Miles of existing telegraph lines used
- Wire size & spacing set 600  $\Omega$  standard
- Transformers & filters made for 600  $\Omega$
- Equipment migrated to radio & recording
  - The “600  $\Omega$  legend” just won’t go away!

# Where Did We Go Wrong?

- TRANSFORMERS were essential elements of EVERY balanced interface 50 years ago ...
- High noise rejection was taken for granted but very few engineers understood why it worked
- Differential amplifiers, cheap and simple, began replacing audio transformers by 1970
- Equipment specs promised high CMRR, but noise problems in real-world systems became more widespread than ever before ...
  - Reputation of balanced interfaces began to tarnish and “pin 1” problems also started to appear!

# Common Mode? Normal Mode?

- Voltages, to ground, that are equal at both inputs are called **common-mode**
  - Voltage between driver & receiver grounds
  - Voltage induced in cable by magnetic fields
  - Voltage induced in cable by electric fields
- Voltages between the inputs are called “differential” or **normal-mode** (signal)

# Common-mode Rejection

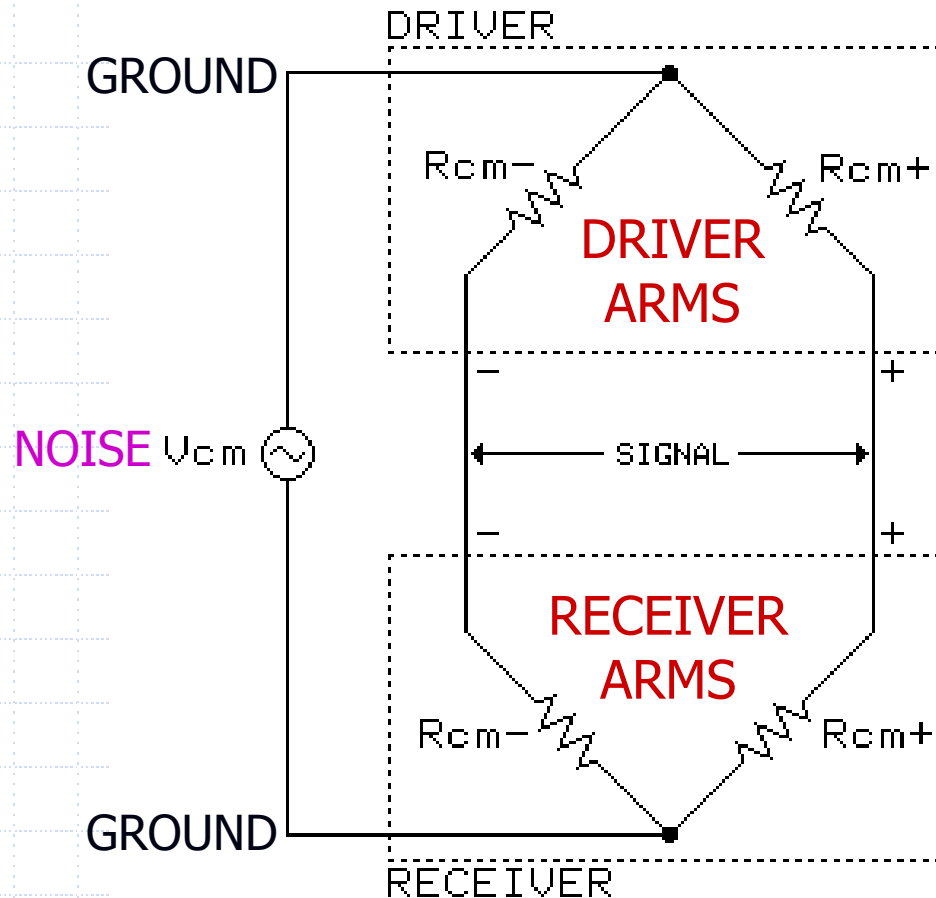
- IDEAL receiver responds only to normal-mode, with no response to common-mode ... it would have infinite Common-Mode Rejection
- Rejection is limited in real-world receivers
- Ratio, in dB, of differential to common-mode gain is Common-Mode Rejection Ratio, **CMRR**
- Noise rejection of the entire interface (what really matters) is highly dependent on how the line and driver affect the receiver!

# The Wheatstone Bridge

- Driver and receiver common-mode impedances form a classic Wheatstone bridge
- Bridge imbalances cause **conversion** of common-mode noise into normal-mode signal
- Balance depends critically on matching ratios of common-mode impedances of the lines
  - **Most** sensitive to component tolerances when driver and receiver arms have same impedances
  - **Least** sensitive when driver and receiver arms have widely differing impedances

**Receiver arm impedances should be very high!**

# A Question of Balance



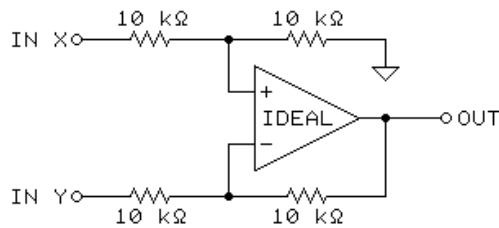
# Blinded by Bad Science

- CMRR traditionally measured with a **perfect** source ... Good marketing but bad science!
- Impedance imbalance at outputs of real audio gear can be  $\pm 30 \Omega$  or more
- IEC recognized inadequacy of their existing CMRR test in 1998 and invited comments
- Whitlock suggested a new procedure that was adopted in August, 2000 as IEC 60268-3
  - Inserts  $10 \Omega$  imbalances, first in one leg and then in the other, of the test signal generator

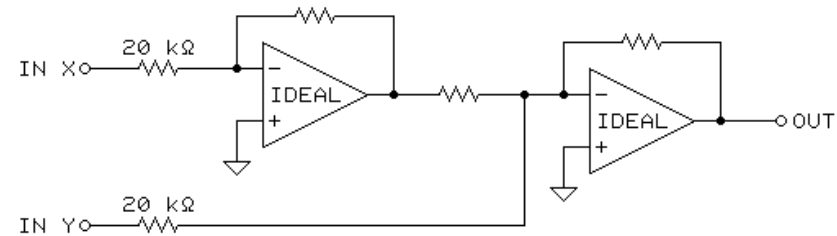


# Conventional Active Input Stages

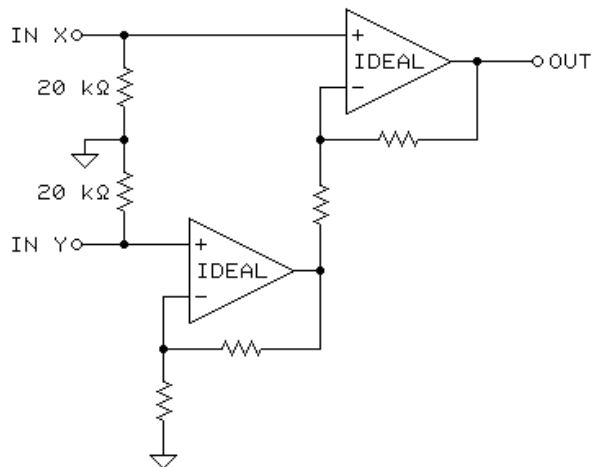
All have  $20\text{ k}\Omega$  common-mode input impedances!



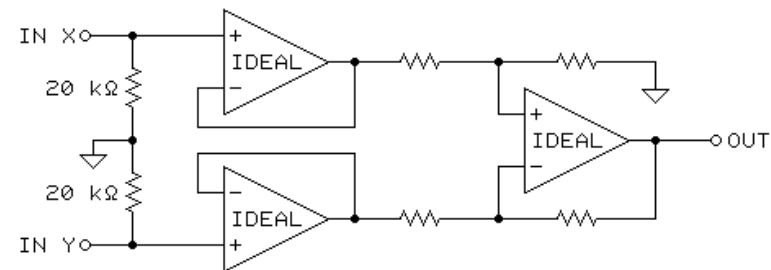
"SIMPLE" SINGLE OP-AMP  
OVER 90% OF ALL BALANCED INPUTS



CURRENT MODE DUAL OP-AMP



VOLTAGE MODE DUAL OP-AMP

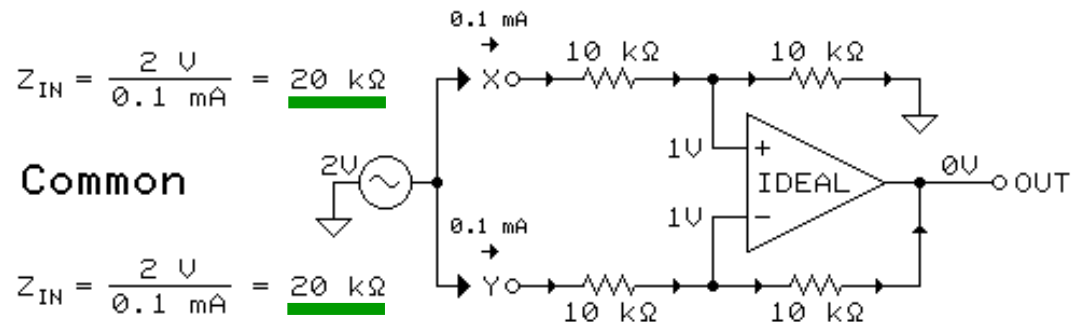
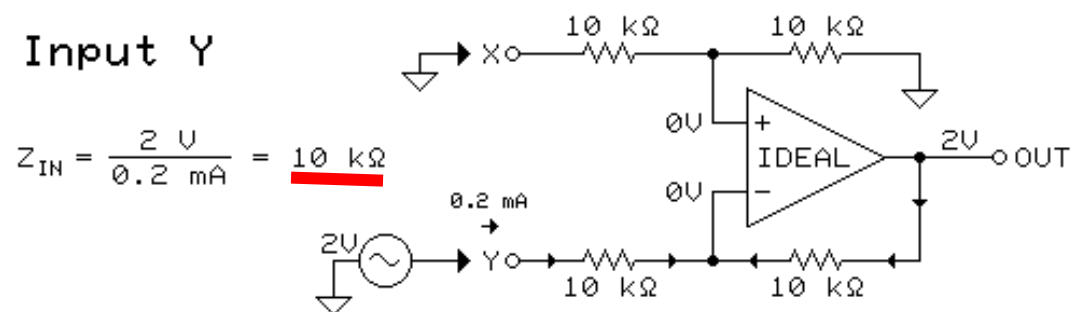
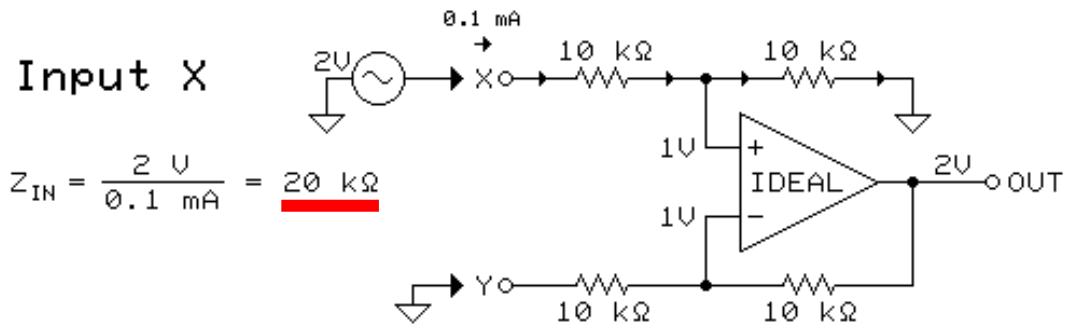


"INSTRUMENTATION" or TRIPLE OP-AMP

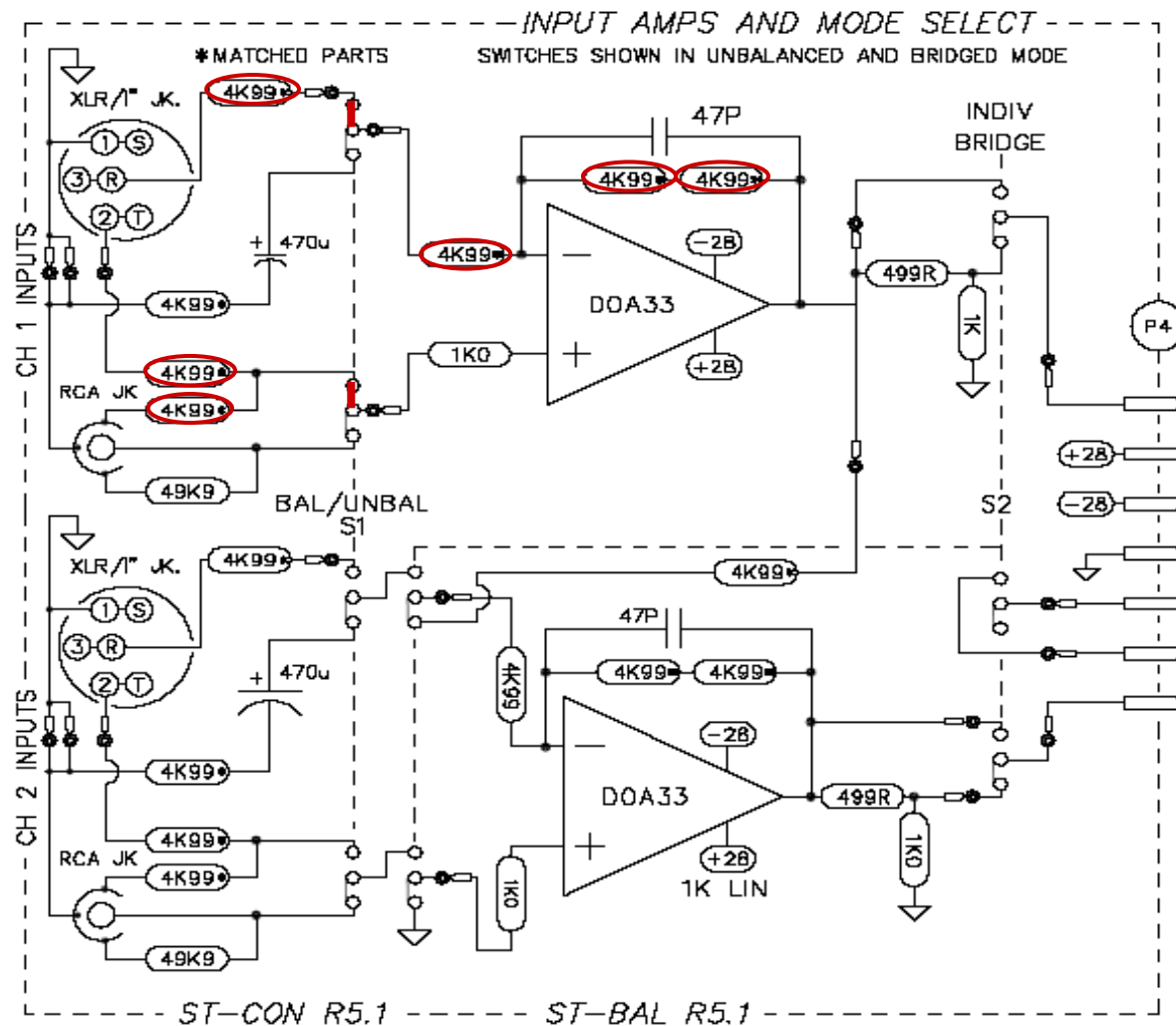
# MYTH: The Diff-Amp Needs Fixing

Driven separately,  
input impedances  
not equal ...  
**NO PROBLEM!**

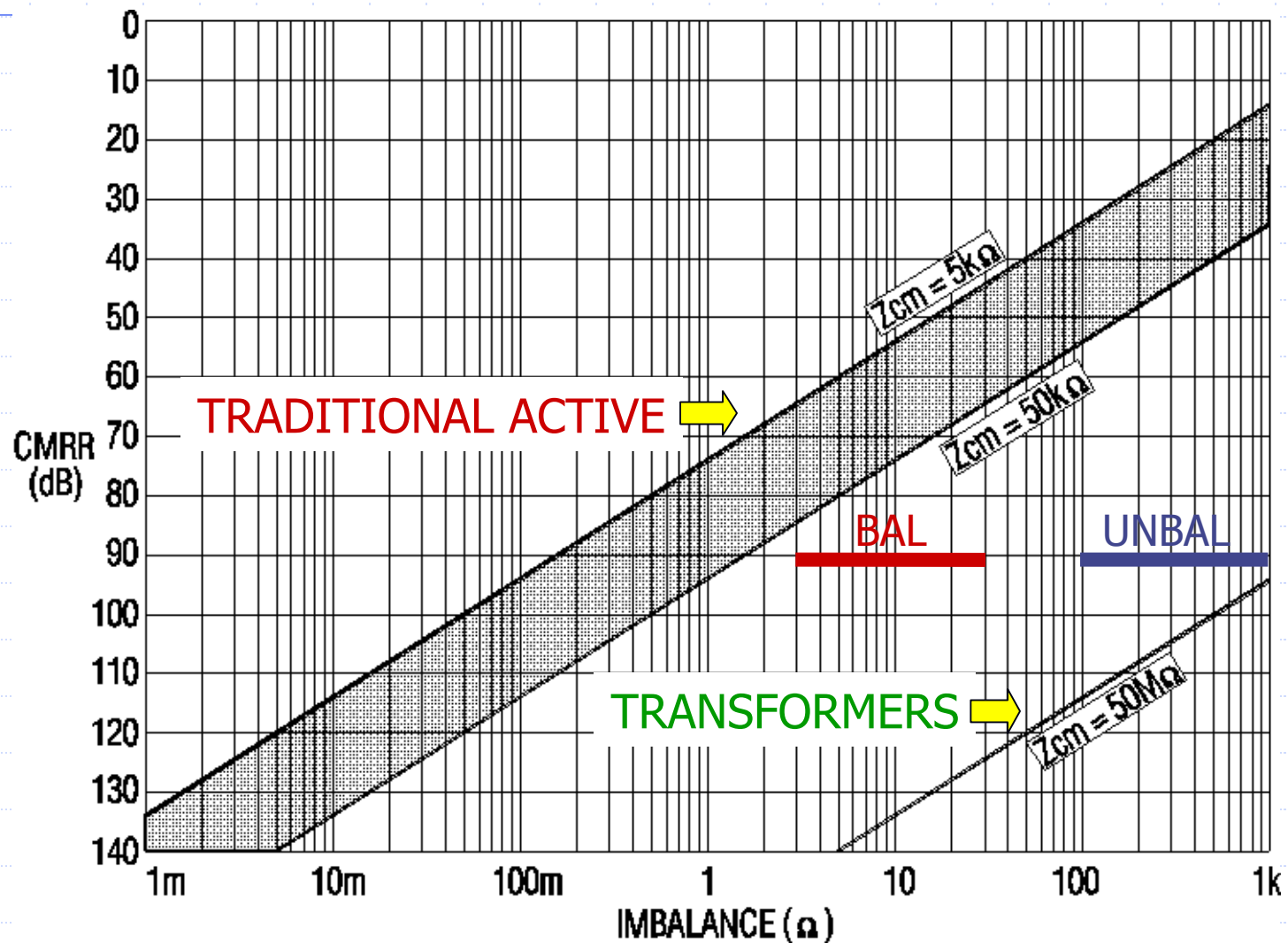
**COMMON-MODE**  
input impedances  
are equal ... OK!



# A Commercial Example



# CMRR vs Real-World Imbalances



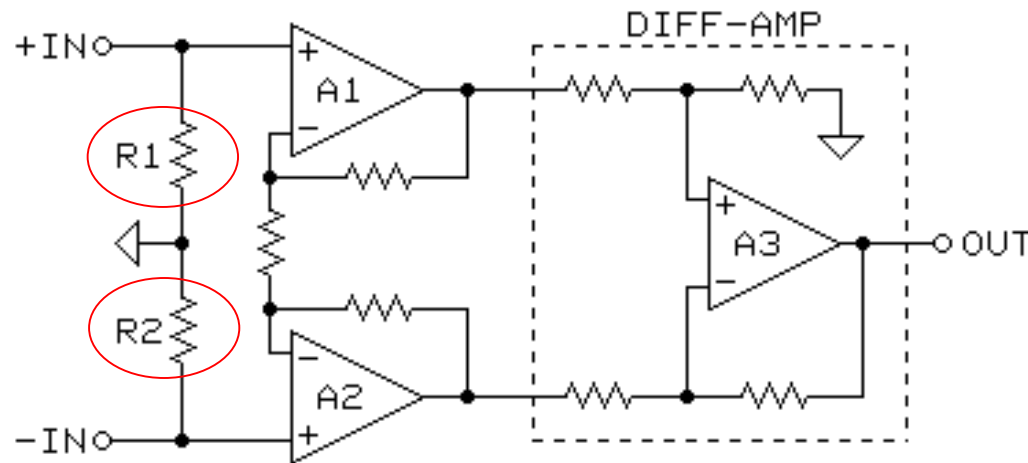
# Why Transformers are Better

- Typical “active” input stage common-mode impedances are 5 k $\Omega$  to 50 k $\Omega$  at 60 Hz
  - Widely used SSM-2141 IC loses 25 dB of CMRR with a source imbalance of only 1  $\Omega$
- Typical transformer input common-mode impedances are about 50 M $\Omega$  @ 60 Hz
  - Makes them 1,000 times more tolerant of source imbalances – full CMRR with any real-world source

# Imitate a Transformer?

Transformer advantage = high common-mode impedances

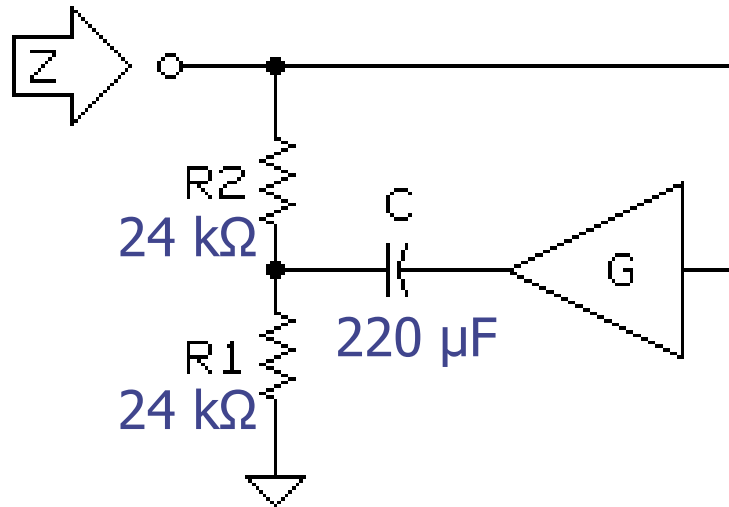
R1 and R2 supply bias current to A1 and A2 but lower input impedances



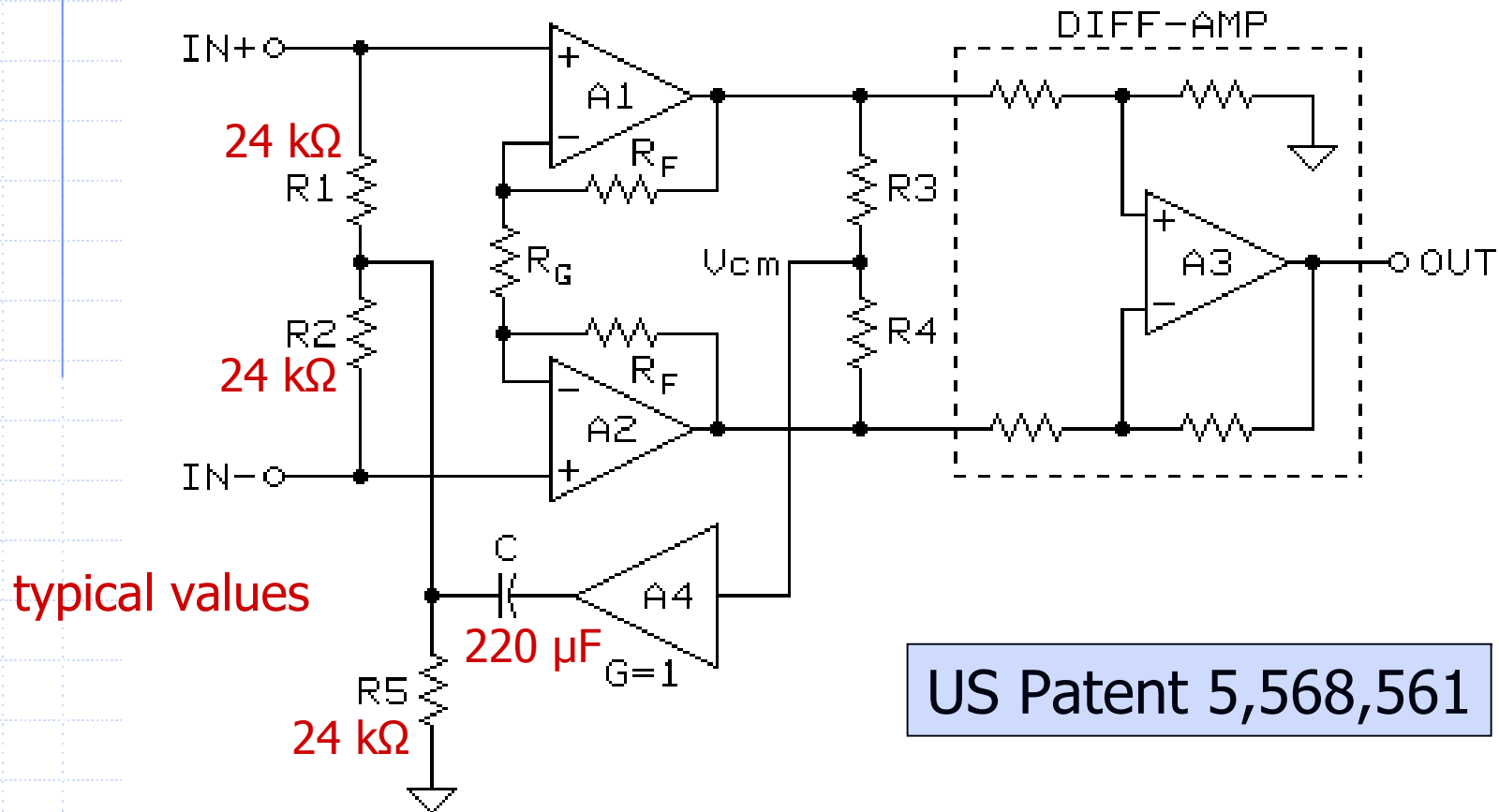
# Up, Up and Away!

“**Bootstrapping**” is a well-known method for increasing ac impedance of resistors

48 k $\Omega$  @ dc  
10 M $\Omega$  @ 60 Hz



# Bootstrapping the Common-Mode





# InGenius<sup>®</sup> Implementation

- R1, R2, and R5 necessary to supply amplifier bias currents (sources may have no dc path)
- CM voltage extracted by R3 and R4
- A4 buffers CM voltage and “bootstraps” R1 and R2 via external C, typically 220  $\mu$ F
- Common-mode input impedances increased to 10 M $\Omega$  at 60 Hz and 3.2 M $\Omega$  at 20 kHz!
- R<sub>F</sub> and R<sub>G</sub> covered by patent for high-gain applications like microphone preamps

# InGenius® IC Design Features

- Fabricated using 40-volt complementary bipolar **Dielectric Isolation (DI)** process
  - High performance NPN *and* PNP **transistors like discretes**
  - High isolation between transistors and no substrate connection
  - Low stray capacitances for **high bandwidth and slew rates**
- Folded cascode op-amp designs with PNP front ends
  - Better noise performance
  - High gain and simple stability compensation
  - Greater input voltage range
- Output driver uses novel, patented output stage

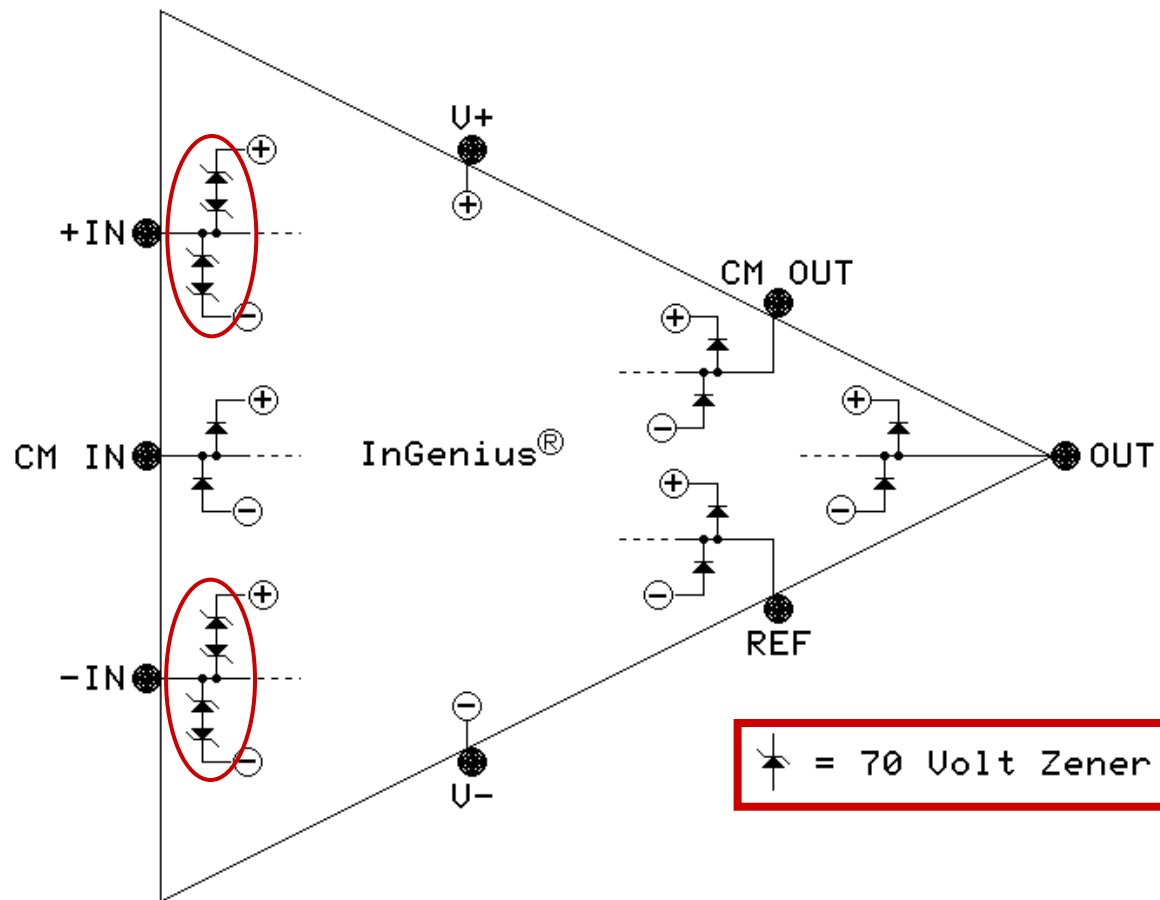
# InGenius® IC Features

- Thin-film Si-Cr (silicon-chromium) resistors utilized
  - Better stability over time and temperature than Ni-Cr (nickel-chromium) or Ta-Ni (tantalum nitride) types
  - Sheet resistance minimizes total die area
  - Accuracy and matching achieved by **laser trimming**
- Resistor matching is critical to CMRR and gain accuracy
  - Match typically within 0.005% ... results in about **90 dB CMRR**
  - Coarse and fine laser trimming optimizes speed and cost
  - This matching both difficult and expensive in discrete designs
  - Accelerated life tests predict >70 dB over life of part

# InGenius® IC Fabrication

- Thin-film resistors vulnerable to electrostatic discharge (ESD) damage
  - Input pins must accept input voltages greater than supply rails, posing an ESD protection challenge
  - New “lateral” protection diode, with typical breakdown of 70 volts, was designed to utilize existing diffusion and implant sequences
- All other pins are protected by conventional clamp diodes to supply rails

# InGenius<sup>®</sup> ESD Protection

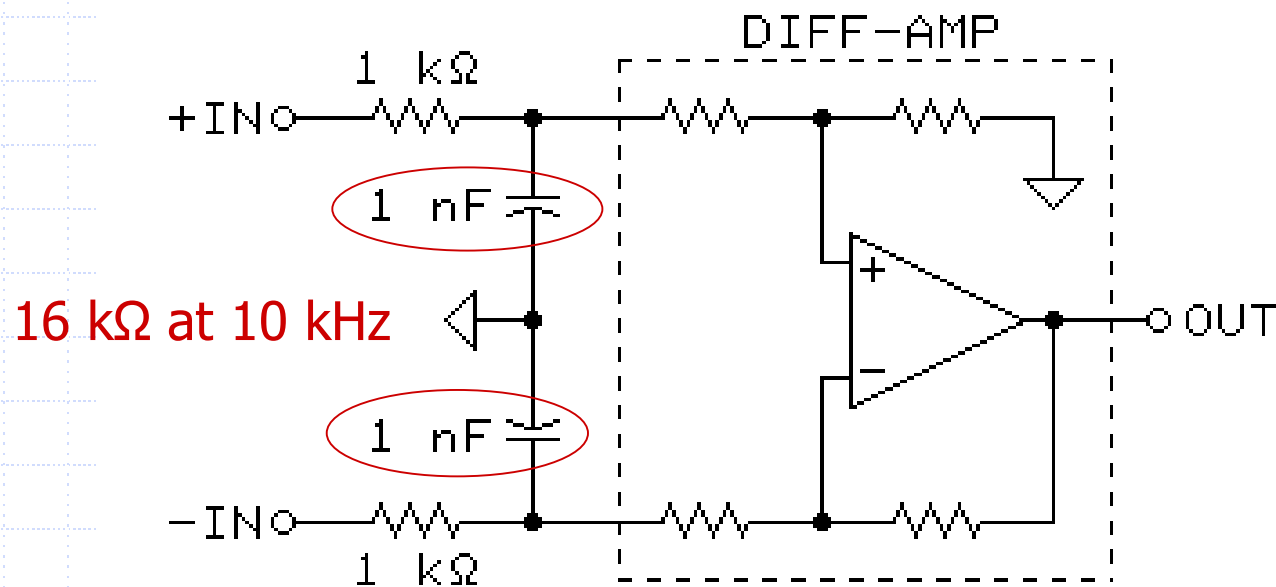


# InGenius® IC Performance

- High CMRR maintained with real-world sources
  - 90 dB @ 60 Hz, 85 dB @ 20 kHz with zero imbalance source
  - 90 dB @ 60 Hz, 85 dB @ 20 kHz with IEC  $\pm 10 \Omega$  imbalances
  - 70 dB @ 60 Hz, 65 dB @ 20 kHz with 600  $\Omega$  unbalanced source!
- THD 0.0005% typical at 1 kHz and +10 dBu input
- Slew rate 12 V/ $\mu$ s typical with 2 k $\Omega$  + 300 pF load
- Small signal bandwidth 27 MHz typical
- Gain error  $\pm 0.05$  dB maximum
- Maximum output +21.5 dBu typical with  $\pm 15$  V rails
- Output short-circuit current  $\pm 25$  mA typical
- 0 dB, -3 dB, -6 dB gain versions = THAT 1200, 1203, 1206

# Traditional RFI Suppression

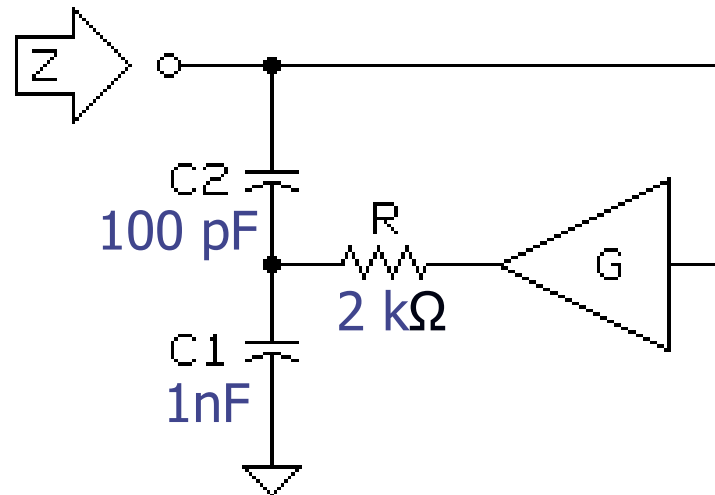
Lowers common-mode  $Z_s$  significantly at higher audio frequencies, which makes CMRR degrade more with source imbalances



# Raising Impedance of Capacitor

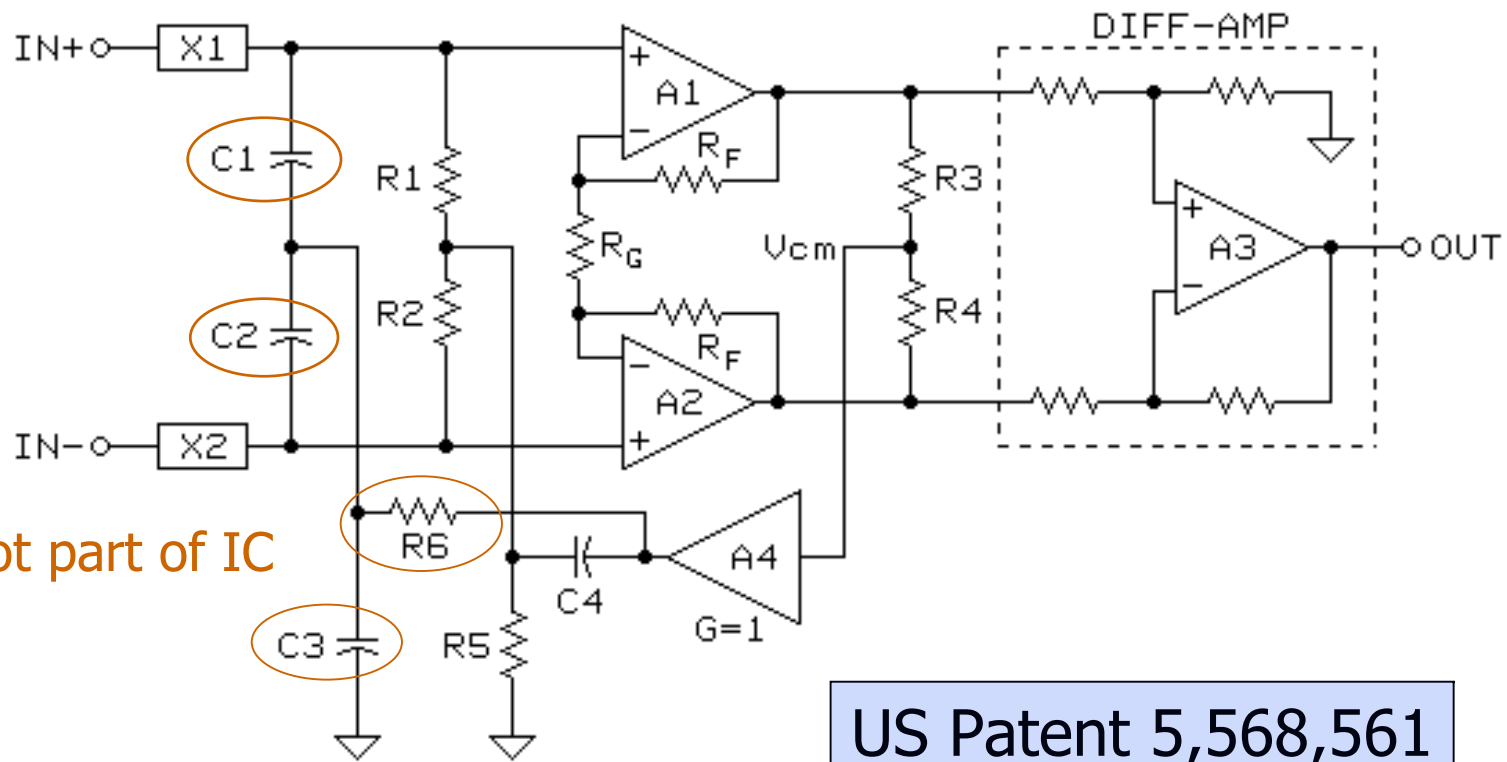
“Bootstrap” lowers effective capacitance of RF filter capacitors at audio frequencies

Effectively **15 pF @ 10 kHz**  
and 91 pF @ 100 kHz





# Bootstrap of RFI Filter Capacitors



# InGenius® Summary

- Conventional active receivers are far cheaper, smaller, and lighter than a quality transformer, but ...
- Transformers consistently outperform them for reasons that need to be widely understood and appreciated
- The main transformer advantage stems from its inherently very high common-mode impedances
- The InGenius® IC exhibits the very high CM impedances previously associated only with transformers
  - Excellent noise rejection even with UNBALANCED sources!
- Its bootstrap feature lends itself to novel and very effective RF interference suppression
- Its high-quality internal op-amps give it **GREAT SOUND**

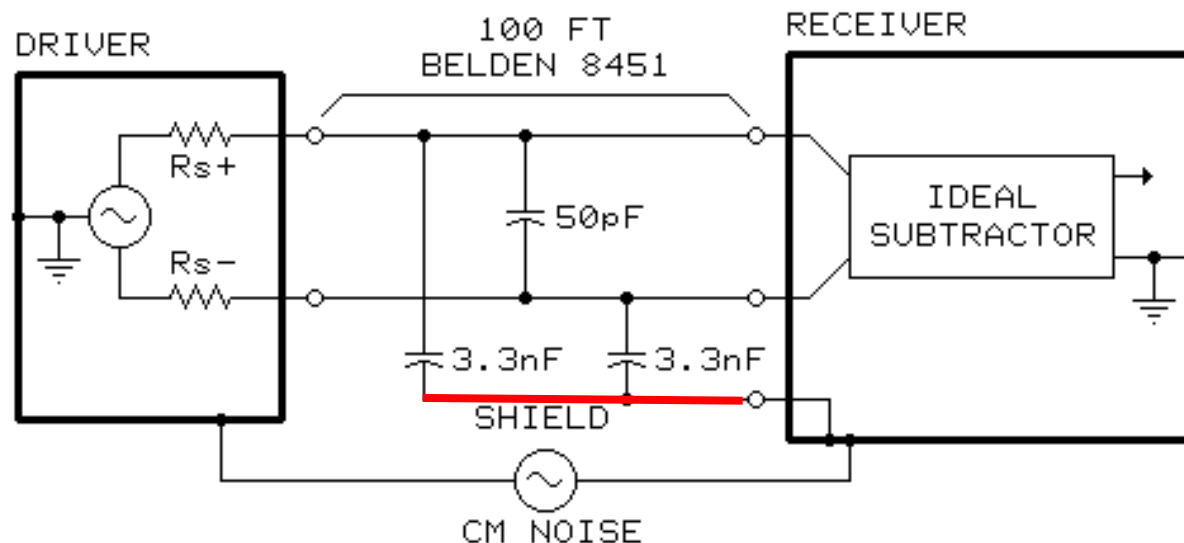
# Balanced Cable Issues

- Capacitance imbalance
- Shielding for electric fields and RF
- Immunity to magnetic fields
- Shield current induced noise (SCIN)

# Shielding

- **Electric** field couples to both signal conductors – coupling may be unequal
  - **Twisting** improves match by averaging physical distances to external field source
- Grounded shield avoids problem by diverting field current to ground
- Braided shield of 85% to 95% coverage is usually adequate

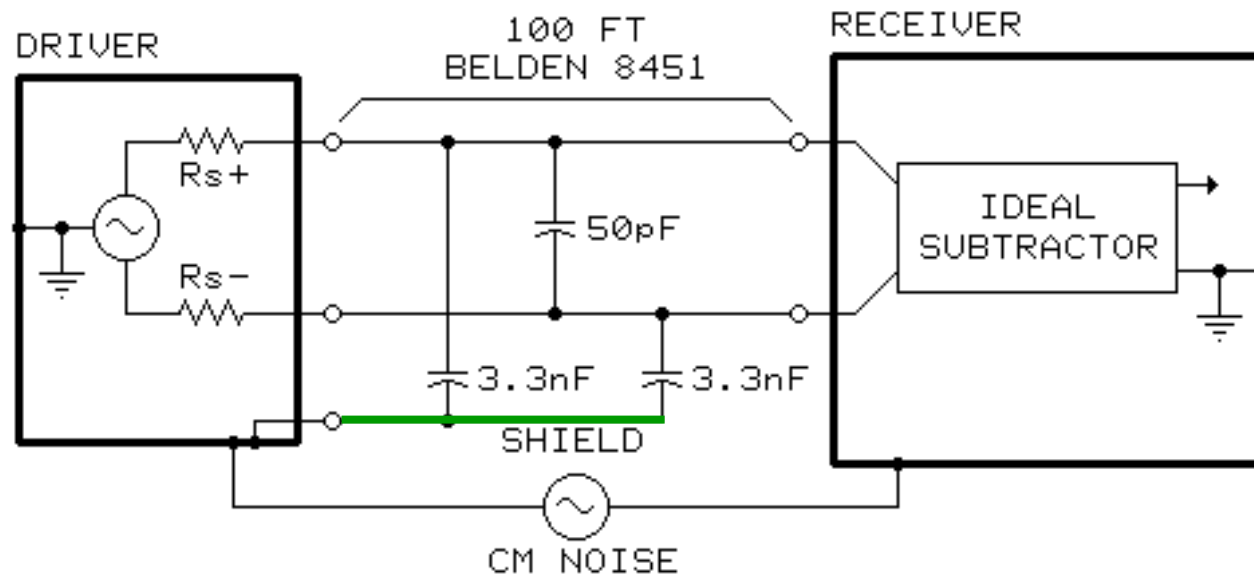
# Ground Only at Receiver = Bad



Forms pair of **low-pass filters** for common-mode noise

- Driver  $Z_o$  imbalances and 4% to 6% typical cable C imbalances create mismatched filters
- Mismatched filters cause **conversion** of common-mode noise to differential, degrading CMRR

# Ground Only at Driver = Good



Grounding only at driver **completely ELIMINATES FILTERS!**  
All filter elements move together (with driver ground)

# Connections and Crosstalk

- Signal asymmetry and capacitance mismatch cause **signal current** flow in the shield
  - Grounding only at receiver forces current to return to the driver via an **undefined** path – **can result in crosstalk, distortion, or oscillation**
  - Grounding only at driver allows current to return **directly** to the driver – **NO PROBLEMS**
- The **driver** end of a balanced cable should **always** be grounded, whether or not the receiver end is grounded

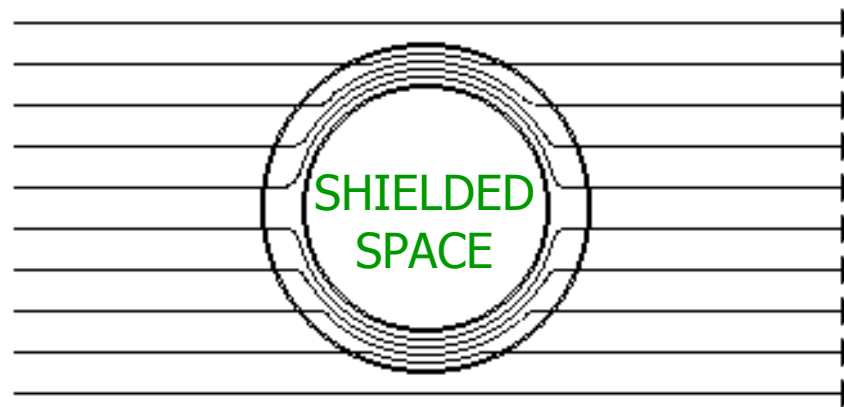
# Common-Mode Voltage Limits

- $\pm 10$  volts (peak) for typical active circuits
  - Total loss of CMR if exceeded = very nasty distortion
- $\pm 250$  volts for typical transformer
  - No audible effect if exceeded (only insulation failure)
- Voltage between driver & receiver ground
  - Less than few volts if both devices grounded
  - Can approach 120 volts if either device ungrounded
  - Shield ground at both ends minimizes
  - Other grounding required in some cases



# Immunity to Magnetic Fields

- Voltages are induced in conductors exposed to ac magnetic fields – voltages may not be equal
  - **Twisting** averages physical distances to external field source
- Effective magnetic shielding at 60 Hz is very difficult
- Only ferrous metals (steel conduit) are low-frequency magnetic shields — **ordinary cable shielding is not**



# Shield Current Induced Noise

- Any current flow in shield creates magnetic field extremely close to the twisted pair
- Slightest imperfections in cable construction result in **unequal** induced voltages
  - Dubbed SCIN in 1994 paper by Neil Muncy
  - **Best** cables use braided or dual counter-wrapped spiral shields and **no drain wire**
  - **Worst** cables use a **drain wire**, regardless of other construction details *[Brown-Whitlock paper]*

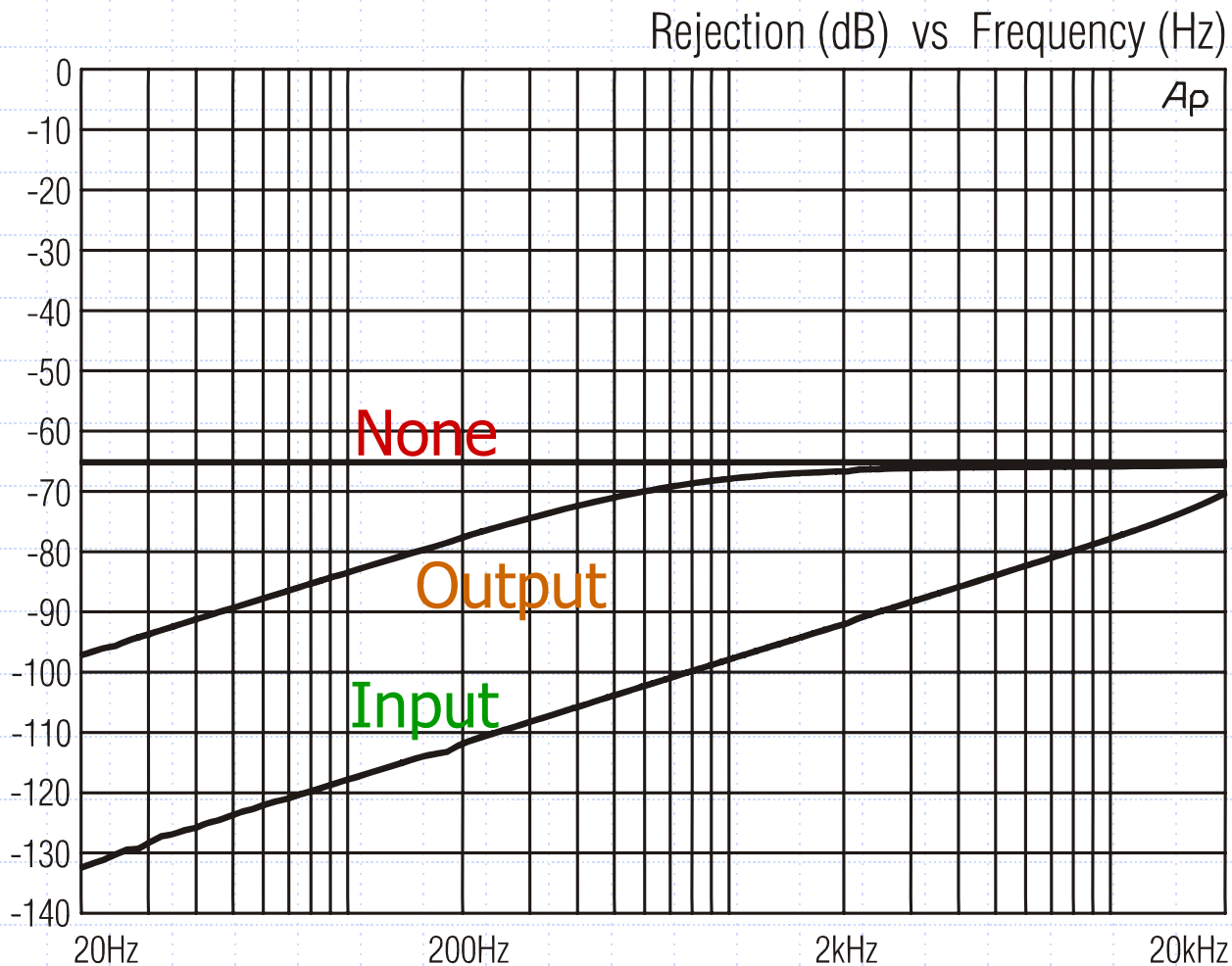
# Isolators for Balanced Audio

- Top problems in “pro” equipment:
  - “Pin 1” problems
  - Poor real-world CMRR
- This isolator solves both
  - DIP switches reconfigure shield connections
  - Faraday-shielded **input** transformers add CMRR



switches on bottom

# Transformers Improve CMRR



IEC CMRR test  
of advertised  
"90 dB CMRR"  
balanced input

# Transformer Performance

- Beware “weasel-words” & “market-speak”
  - Missing specs or unspecified test conditions
  - Level handling & distortion rated at 50 Hz
- Jensen data complete and user-verifiable
  - Sonic transparency is our design goal
  - Level handling & distortion rated at 20 Hz
    - High level, low frequency distortion most telling
  - Phase distortion (deviation from linear phase) specified for every part we make

# A Balanced Checklist

- **Keep balanced line pairs tightly twisted**
  - Immunity to magnetic fields
  - Especially important in low-level mic circuits
    - Terminal blocks and XLRs vulnerable to magnetic fields
    - "Star-Quad" mic cable reduces magnetic pickup 40 dB
  - Immunity to electric fields for unshielded pairs
- ◆ Grounding of cable shields is important
  - **Always** ground at the driver
  - **OK** to ground at both ends
  - **Never** ground **only** at the receiver

# Unbalanced to Balanced Audio

- AKA "Consumer to Pro"
- Reference signal levels are different
  - Consumer ref = -10 dBV = 0.316 V rms
  - Professional ref = +4 dBu = 1.228 V rms
  - Takes voltage gain of about  $4\times = 12$  dB
- Use a 1:4 step-up transformer?

# It Seems Like a Good Idea ...



*Rane Corp.*

Uses 1:4 step-up transformer

- ▶ 1:4 turns ratio transformer reflects impedances at 1:16 ratio
- ▶ Consumer output drives 625  $\Omega$  to 2.5 k $\Omega$  load (not recommended)
- ▶ Headroom, distortion, and frequency response are degraded
- ▶ Actual gain becomes 3 to 8 dB

**NOT** a good solution ...

12 dB of gain “reach” is normally available at the balanced input



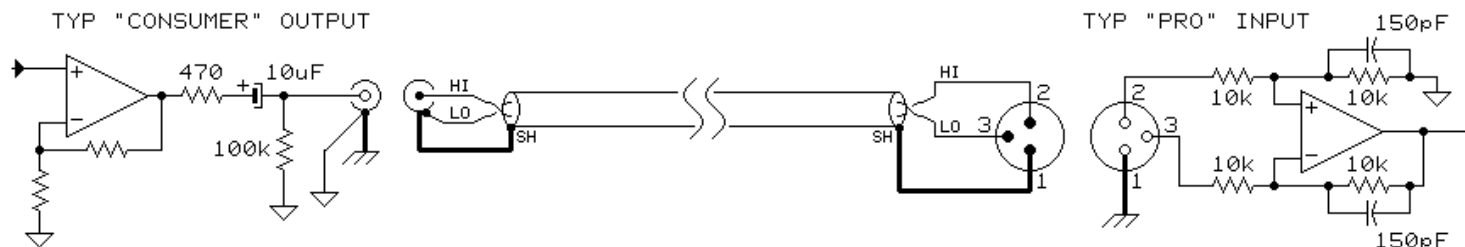
# Simple but Smart

- Noise rejection is usually issue, not gain
- Use of 2-conductor cable invites noise due to common-impedance coupling
- Use of 3-conductor cable stops ground noise current flow in signal conductors!
  - If input uses transformer or InGenius® IC, rejection can be up to 100 dB

# 2 Conductors or 3?

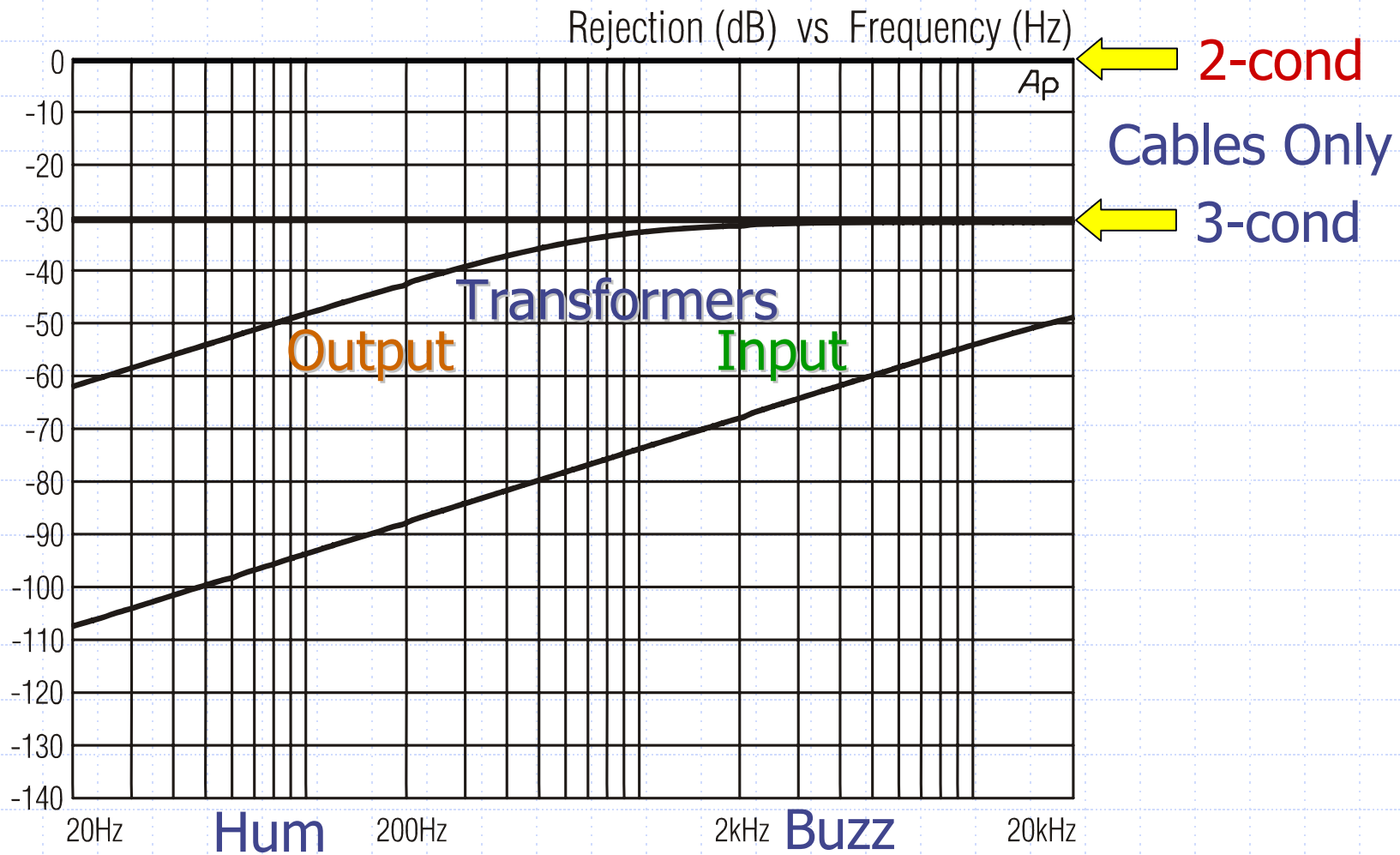


2-c cable and adapter results in **NO** rejection at all



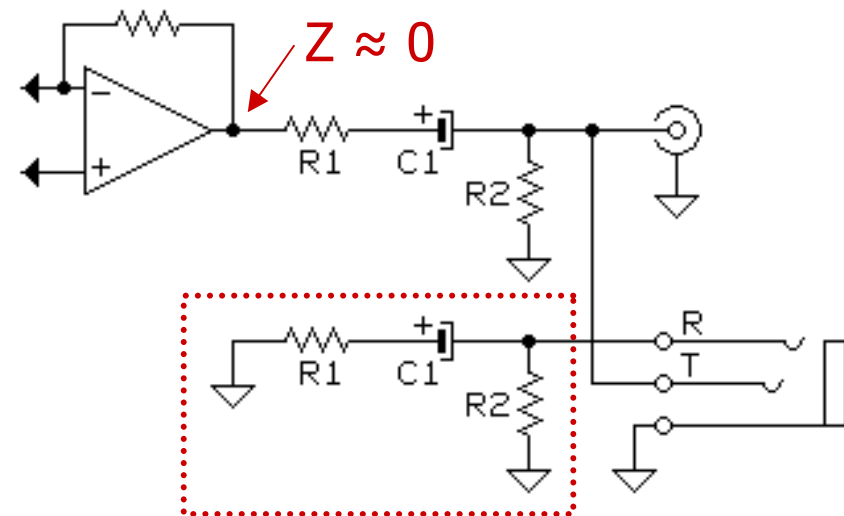
3-c cable results in **30 dB** rejection for typical input

# Relative CMRR Performance



# “Universal” Consumer Output

- True Balanced Out on TRS (or XLR)
- Unbalanced Out on TS or RCA
- Simultaneous Use Causes Imbalance

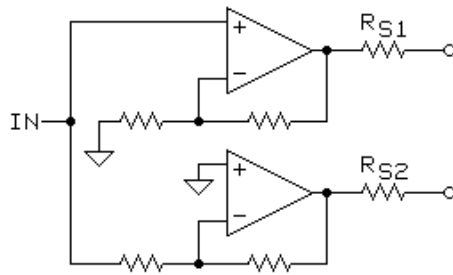


DUPLICATE OF EXISTING  
OUTPUT NETWORK

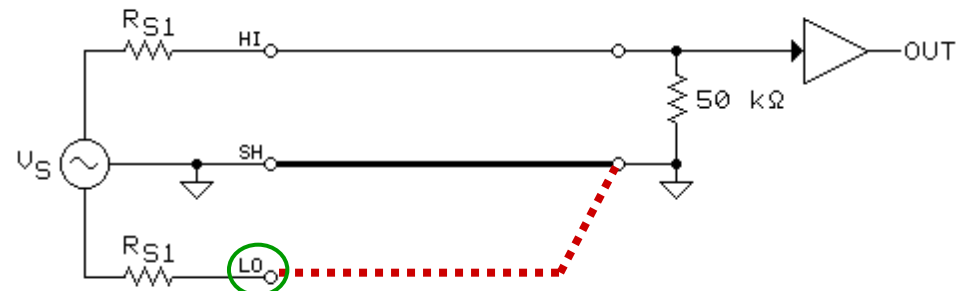
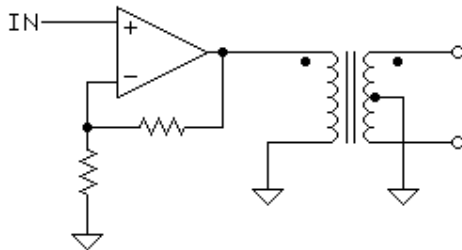
# Balanced to Unbalanced Audio

- AKA “Pro to Consumer”
- Signal level difference is legitimate concern
  - Consumer inputs easily over-driven by pro levels
  - Requires voltage loss of 12 dB
  - Lower pro output? – metering & noise degrade
- One wiring method will NOT work for all kinds of line output circuits – it’s risky business!

# Ground-Referenced Symmetrical



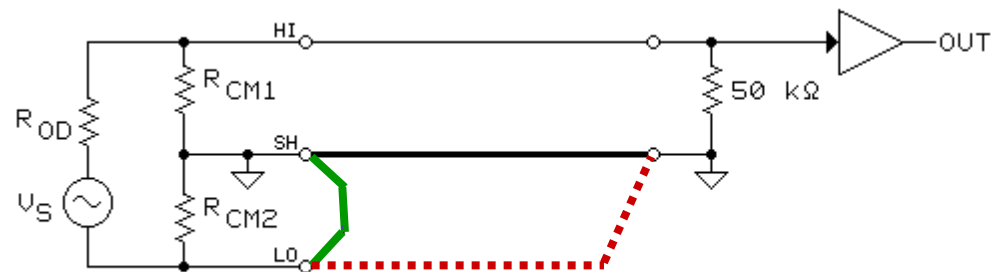
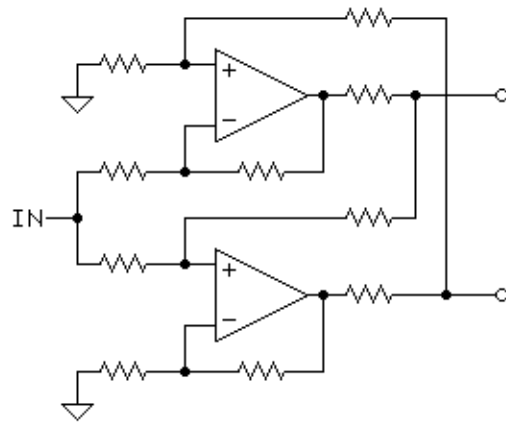
OR



Equivalent Circuit with Unbalanced Receiver

- Driver “unhappy” when either output is grounded
- Unused output must float
- No noise advantage over unbalanced output

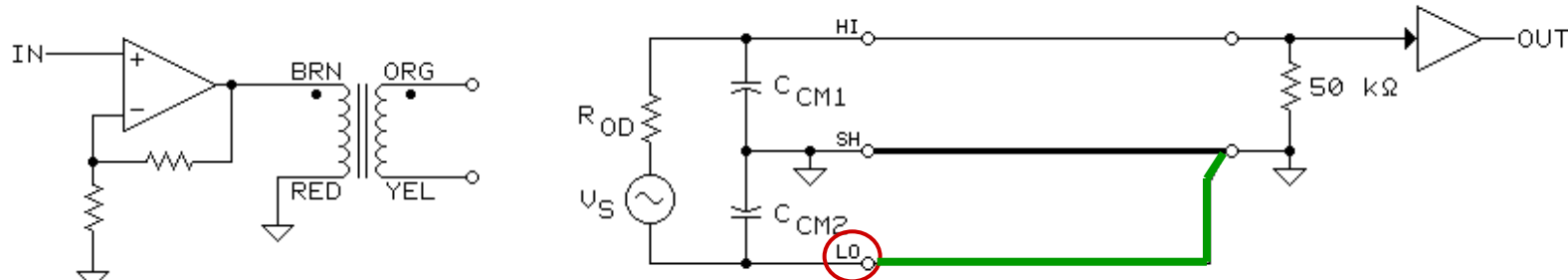
# “Active Balanced” Floating



Equivalent Circuit with Unbalanced Receiver

- Either output can be grounded, but **only at driver**
  - Grounding at receiver can make driver unstable or oscillate
- Large level loss if one output left floating
- Identical to unbalanced for noise susceptibility

# Transformer Floating

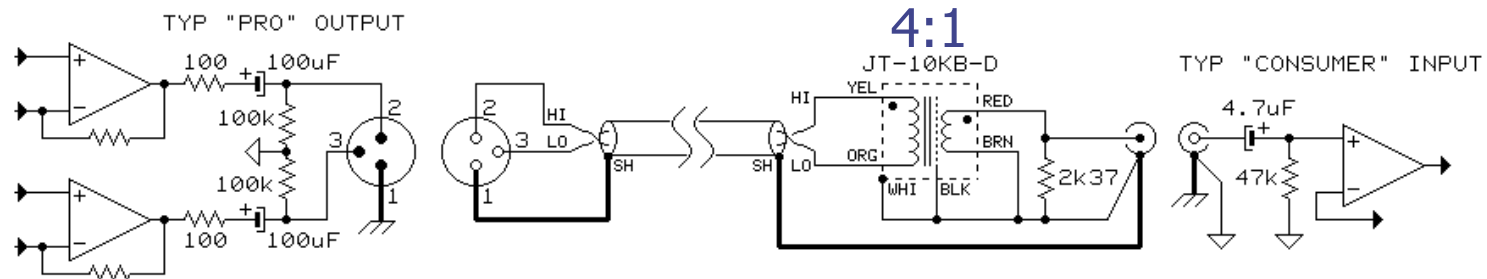


Equivalent Circuit with Unbalanced Receiver

- Either output can be grounded – anywhere
- Grounding at receiver gives 70 dB hum improvement
- Low-frequency loss if either output floats!!
  - Also applies to transformer-balanced inputs, regardless of driving source, if either input floats!!

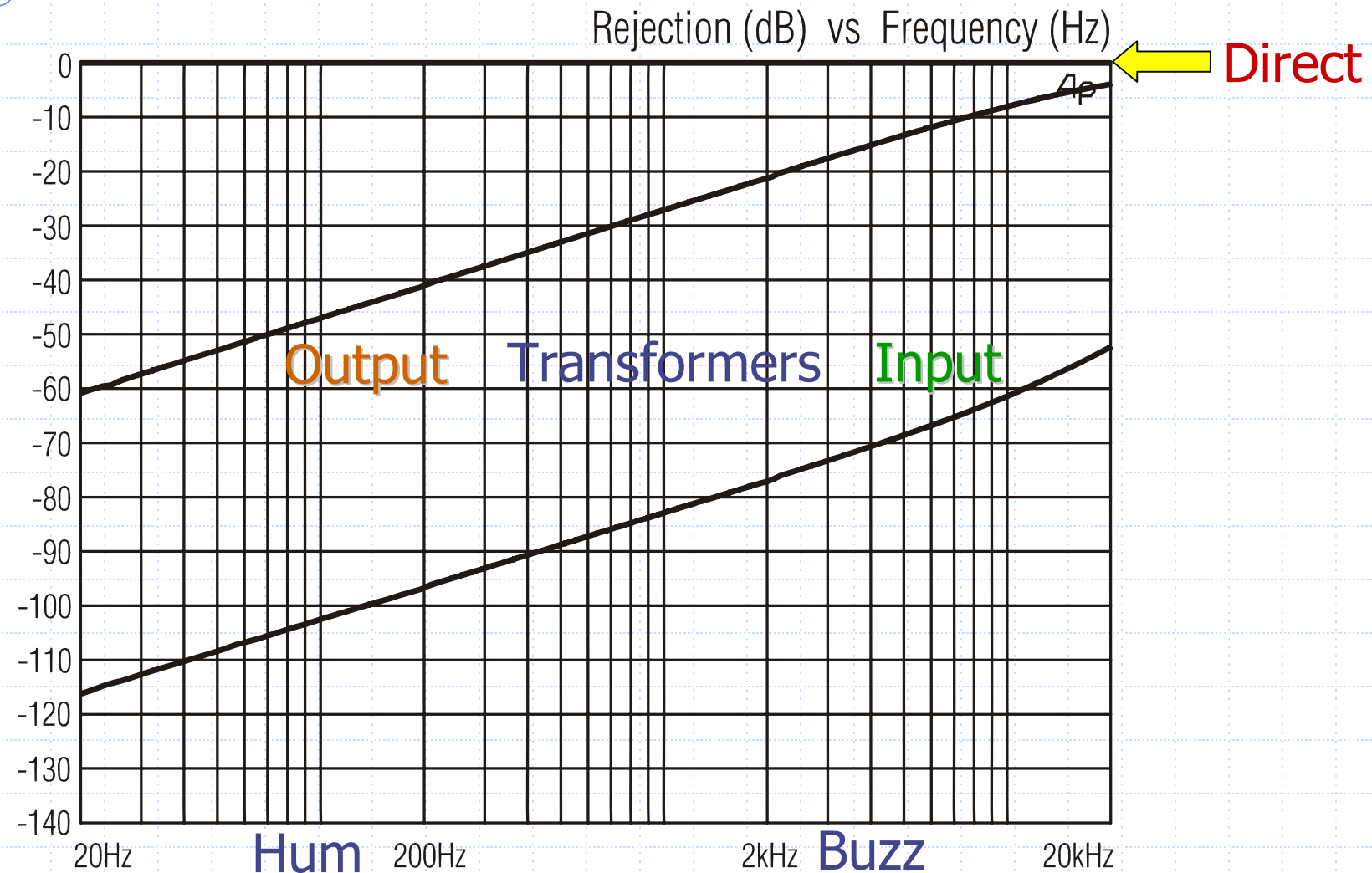


# Don't Worry, Be Happy



- Works with **any** variety of output stage
- Transformer attenuates signal 12 dB
- Superior ground noise rejection

# Relative CMRR Performance



# Thanks for Your Attention!

"Handbook for Sound Engineers"  
includes Whitlock chapters on:

- ▶ Audio Transformers
- ▶ Microphone Preamplifiers
- ▶ Grounding and Interfacing

Think of a question later?  
[whitlock@jensen-transformers.com](mailto:whitlock@jensen-transformers.com)

